# Strategies and Costs to Exceed ASHRAE 90.1-2004 Requirements in a Multifamily Apartment Building

#### **Prepared for**

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# Strategies and Costs to Exceed ASHRAE 90.1-2004 Requirements in a Multi-family Apartment Building March 2008

#### **EXECUTIVE SUMMARY**

#### Scope

Recent proposals to increase requirements by 30% to 50% over today's energy codes and standards may have a dramatic impact on certain types of multi-family buildings. Apartments, already some of the most sustainable residential buildings given their high density and efficient building systems, are of particular interest because of the role they play in providing affordable housing.

This study addresses how increases in energy efficiency standards will impact apartments in selected locations – Chicago, Houston, and Atlanta. These cities were selected to investigate impacts across multiple climate zones. Further, construction practices and infrastructure to support market preferences vary across these cities.

In this study, we focused on technologies and building systems which would be needed to surpass the 2004 edition of ASHRAE 90.1 – "Energy Standard for Buildings Except Low-Rise Residential Buildings" by 15%, 30%, and 50%. The technology packages which were modeled were in keeping with the realistic limits of what can be accomplished in building assemblies with commercially available envelope and HVAC systems.

#### Standard and Modeling Background

ASHRAE 90.1 is perhaps the most widely adopted energy conservation standard in the United States. As the title indicates, this standard regulates energy performance in a wide range of commercial buildings as well as some residential buildings. It is frequently referenced as an alternative compliance option in other energy codes, including the International Energy Conservation Code (IECC).

The most direct way to identify how a building performs relative to ASHRAE 90.1, or any other code, is to conduct computer simulations on a proposed building design and then compare it to a base code-compliant building. ASHRAE 90.1 offers a method called the "cost budget method" that permits this approach using energy simulation software. We selected a software package for the primary simulations called Energy Gauge Premier Summit Version 3.11, distributed by the University of Central Florida's Florida Solar Energy Center. Energy Gauge is somewhat unique in that it automatically generates a reference code-compliant building based on the inputs that a designer uses for their proposed design. The reference building design represents the costs that a building would incur for the items covered by 90.1 if the building is designed to comply with the *minimum* requirements of the standard. By automatically creating this reference building, this software tends to reduce user bias, which can be significant in modeling the energy use of the reference building.

#### **Energy Simulation Results**

The results of the energy simulations conducted in this project demonstrate significant barriers to reaching different levels of efficiency relative to the 2004 ASHRAE 90.1 standard. Table ES1 shows the reference design annual energy cost budget generated for a four-story building with 32 apartments of approximately 1000 square feet each.

Table ES1 - Annual Energy Costs for Reference Buildings

	Atlanta 90.1 Reference	Chicago 90.1 Reference	Houston 90.1 Reference
Electricity	\$32,946	\$25,323	\$64,960
Natural gas		\$31,628	
Total Cost Budget	\$32,946	\$56,951	\$64,960

The total cost budget in Table ES1 is the starting point. To improve upon a building's performance, a building would have to incur a lower total cost budget than shown in the table. Note that Chicago's costs include natural gas for a hot air furnace whereas electric heat pumps are more typical in Houston and Atlanta.

### Improvements to the Building Envelope Provide only Modest Gains

Because improvements to the opaque envelope (walls, roofs, floors) are typically the first items targeted for code changes, it is important to understand how they could impact the performance of a building. The chart below illustrates selected envelope improvements from the simulations in Atlanta. Most envelope improvements, when assessed in isolation, provided less than 1% energy savings. Even combining multiple improvements to the envelope resulted in less than a total of 2.5% improvement. Similar results were found in Chicago and Houston. The only exception seems to be the addition of R-5 subslab insulation in Chicago, which produced about a 3-1/2% savings over R-0 subslab insulation.

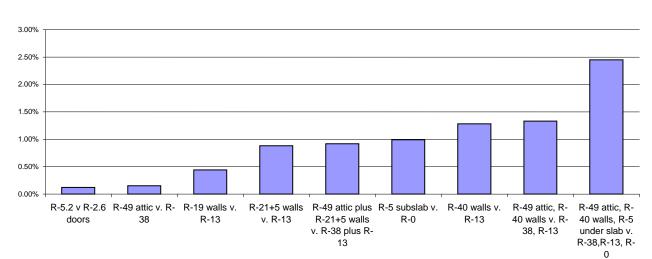


Figure ES1 - Improvement due to selected component changes over base building (Atlanta)

It is not possible to save the same energy multiple times, so it is not accurate to simply add the results of different simulations to arrive at a combined savings estimate. The different systems tend to interact with each other. Thus, only when multiple options are evaluated simultaneously in a simulation do the results reflect their combined contribution.

From Figure ES1, it became obvious that the traditional approach of adding more and more insulation would not get us very far toward the goals of 30% and 50% improvement. More emphasis has to be placed on higher efficiency heating and cooling equipment.

### Significant Better-than-Code Gains Require Significant HVAC Upgrades

Table ES2 shows the results of the most promising options and the highest levels of improvement that were obtained. Note that a specific building configuration would not always provide exactly 15%, 30% or 50% improvements. Thus, the table shows the options that are enough to surpass the stated goals, but they often go beyond the goal.

Missing from the table is an entry close to the 15% threshold for Atlanta. This is because none of the options we explored could reach this goal without moving up to a ground source heat pump (GSHP), and this technology provided such a significant improvement that it met both the 15% and 30% thresholds in Atlanta.

Table ES2 - Building System Packages to Exceed 90.1 Requirements for three U.S. Cities

Atlanta	% better than 90.1
GSHP (3.7 COP, 16.9 EER)	31
R-49 attic, R-21+5 walls, advanced windows (U=0.3, SHGC=0.19), R-5.2 door, R-5 subslab insulation, GSHP (COP 3.7, EER 16.9)	39
Chicago	
96 AFUE furnaces	15
GSHP (3.7 COP, 16.9 EER)	37
R-49 attic, R-40 walls, R-5 subslab insulation, GSHP (3.7 COP, 16.9 EER)	46
Houston	
SEER 15 HP w/ 8.3 HSPF, R-40 walls, R-49 attic, advanced windows (U=0.3, SHGC=0.19)	15
GSHP (3.7 COP, 16.9 EER)	41
R-40 walls, R-49 attic, advanced windows, GSHP (3.7 COP, 16.9 EER)	48

None of the improvements we explored were able to achieve the 50% goal, although the modeling for Houston approached this threshold. Reaching the 15% threshold in Houston and Chicago was achievable by using high efficiency conventional HVAC equipment. For the 30% level in Houston and Chicago, as well as the 15% level in Atlanta, only the use of a GSHP allowed the efficiency goal to be reached.

#### Payback Periods for the Required Upgrades present Challenges

To illustrate the potential impact on costs and payback, Table ES3 shows these values for the building simulations in Atlanta.

As mentioned earlier, GSHPs played a significant role in meeting many of our performance goals. These systems come with a significant increase in upfront cost. It many cases, the payback period for this technology will exceed the life of the system, or at least the time when significant replacement components are needed.

Table ES3 – Cost and payback for selected improvements in Atlanta

Building system package	% better than 90.1	Simple payback in years <sup>1</sup>
	31 (closest set of	16 (25)
	improvements achieving at	
GSHP (3.7 COP, 16.9 EER)	least 30%)	
R-49 attic, R-21+5 walls, advanced windows (U=0.3,		14 (21)
SHGC+0.19), R-5.2 door, R-5 subslab insulation, GSHP	39 (maximum achieved in	
(COP 3.7, EER 16.9)	simulations)	

<sup>&</sup>lt;sup>1</sup>Costs and thus payback of GSHPs vary greatly. The paybacks are based on an average of the high and low end of estimated costs. The payback associated with the high end of the cost estimates is shown in ().

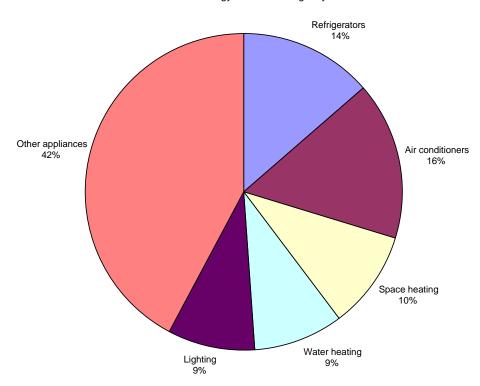
# ASHRAE 90.1 Does Not Cover All Building Energy Use, Which Limits the Ability to Reach Better-than-Code Efficiency Targets

It is important to understand that not all of a building's energy use is regulated in ASHRAE 90.1. For example, lighting within dwellings is outside the scope of 90.1. Likewise, the energy use associated with water heating in an apartment is not covered. Appliance energy is also not regulated by the standard.

Figure ES2 shows the electric energy use in residential buildings as a way to illustrate where energy is used in a building. This demonstrates that even if codes and standards like 90.1 are made to be 30% or 50% better than today, the overall impact on total energy use would be substantially less in a building like an apartment. This is because 90.1 does not directly address items like appliances and refrigerators that make up a large part of a residential building's energy use.

Figure ES2 – Residential electricity by end use (2001)

Source: US. Energy Information Agency RECS data



# On-Site PV Systems could Allow Buildings to Meet the 50% Goal, but are Costly and are not within 90.1's Scope

If the scope of 90.1 were broadened to capture more energy uses, it might be possible to reach the 50% goal in each city by generating electricity at the site through the use of electric photovoltaic (PV) systems or other renewable energy. Assuming that PV was recognized by ASHRAE 90.1, the costs to make up the gap between the highest levels of efficiency realized in the modeling and the 50% goal are shown below. Because there are wide ranges of costs associated with specific PV systems, a range is shown in Table ES4.

Table ES4 - PV System Cost Estimates to Supplement Other Technologies and Meet 50% Threshold

	Atlanta	Chicago	Houston
Normalized low-end cost of installed system (\$/W DC)	\$7.00	\$7.00	\$6.00
Normalized high-end cost of installed system (\$/W DC)	\$9.00	\$9.00	\$8.00
Total low-end cost of PV system (\$)	\$240,885	\$154,778	\$42,527
Total high-end cost of PV system (\$)	\$309,709	\$199,000	\$ 56,703

There may be options other than PV that can be used to make up the deficits in each location. In any case, applying them in an effort to meet better-than-code targets would require significant change to the ASHRAE 90.1 scope. If for example, lighting for dwelling units were added to the scope for the standard, then something as simple as using CFLs might provide enough savings to reach the 50% threshold in Chicago and Houston. Other improvements such as high efficiency water heaters would likely be needed in Atlanta.

#### **Conclusions**

Specific conclusions from this study include the following:

- The 30% and 50% "better than ASHRAE 90.1" levels will clearly present some practical and cost barriers for designers, builders and owners. In fact, it will be nearly impossible to reach the 50% level for an apartment building of the type studied in this project with today's technology without some type of scope change to the 90.1 standard to allow credit to be taken for improvements in energy uses not currently regulated by the standard.
- Even in climates or with buildings where it may be possible to reach the 50% level, the cost to do so will be significant. Most likely, a building will need to be fitted with GSHP technology, which in many areas does not have a well developed support infrastructure at this time to support the number of buildings in question. The cost to use GSHPs in the building we simulated could be several hundred thousand dollars over conventional equipment used in today's buildings.
- The simple payback to achieve an improvement over ASHRAE 90.1 of 30% or higher is likely to be outside of the range that would normally be accepted for this type of analysis. For example, the average payback of about 16 years for the 30% improvement level in Atlanta is somewhat excessive. Furthermore, this is only an average payback. Some buildings could be penalized with paybacks as high as 25 years depending on the local cost of items such as GSHPs, which vary greatly.
- The costs associated with reaching the 30% and 50% performance levels would be nearly impossible for a builder or owner to recapture. Increased rents would be hard to realize when renters have a choice of lower cost, older apartments – which would also tend to be less efficient. Conversely, the energy savings would accrue to the renter in a newer building where most utilities are paid by the renter. This disconnect needs to be considered in any cost benefit analysis before modifying codes and standards.
- Traditionally, energy codes and standards have targeted increased levels of
  insulation as the primary method for increasing a building's performance.
  Additional insulation offers diminishing returns almost all increases will improve
  the building by less than 1%, and most by only a fraction of a percent. Even
  when insulation levels in all of the major components of a building (roofs, floors,
  walls) are increased simultaneously, they do not begin to come close to reaching
  even the 15% threshold.

- Designers will need to specify high efficiency equipment to make significant gains in building performance. In most cases, this should be the starting point rather than additional insulation since the costs of additional insulation can be significant and the benefit very small.
- Changes to the 90.1 scope could help designers and builders to more easily reach the proposed increases in performance. For example, it would be easy and not very costly to use CFLs in lighting fixtures and save a significant amount of energy in an apartment. Currently, the 90.1 standard exempts the inside of dwelling units from the lighting requirements. There may be good reasons for this exemption related to enforceability, but if the standard allowed a designer to submit to the lighting requirements, it would provide an opportunity for them to move closer to the 30% or 50% levels. Appliances, water heaters, and air leakage (infiltration) are other items where similar opportunities exist.
- Onsite generation of renewable energy also could help a designer to reach the 30% or 50% performance levels. As with lighting, the 90.1 standard would need to be revised to allow for any electricity generated by PV, wind, or other systems to offset energy costs in the 90.1 energy cost budget method.
- The methods used in this study relied heavily on building simulations. Simulations are good methods to estimate the *relative* performance of changes to the same building. They should not be used to predict the actual overall energy use of a building, since there are too many factors besides design that influence energy use. Simulation tools have many limitations and require assumptions that introduce a heavy user bias. Further, use of the prescriptive methods in codes and standards is the more typical approach for designing a building. When a simulation approach is introduced, the cost and time for the simulations could be significant. Modeling results from this and similar studies could help reduce the costs by providing designers with a head start in deciding what to simulate.
- Policy makers and codes/standards developers should recognize that the market infrastructure, climate, and consumer preferences all influence the design of a building. Climates and markets can be radically different around the United States. Approaches that seem reasonable in one part of the country should not be automatically adopted elsewhere. For example, just because a high efficiency heat pump may be the best choice for a building from an energy savings perspective, in some climates it is unlikely that homeowners will be accepting of anything but a hot-air furnace system. Forcing them to accept something else could have a negative impact on energy efficiency if they are so accustomed to warmer air that they end up running their heat pump in back-up or emergency electric resistance mode as a way to provide warmer air.
- Overall, for multi-family buildings like the ones analyzed in this project, the
  uniform imposition of higher efficiency standards without scope changes to 90.1
  could have negative, unintended consequences. Builders and owners will
  absorb added costs, yet the building occupants will accrue energy cost savings
  benefits. The required capital for engineering and constructing such buildings

will increase substantially, yet the return on this investment is uncertain at best. Ultimately these dynamics could undermine the viability of new high-performance multi-family buildings and instead push the market towards the continued use of older, far less efficient dwellings.

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#### **DEFINITIONS AND TERMINOLOGY**

<u>AC</u> – Acronym for air-conditioner. In this study, we assumed that a building can be cooled by either a separate electric AC system, or by a heat pump.

<u>Air-source Heat Pump</u> – A heat pump is a technology that provides both heating and cooling using a single compressor for both purposes. An air source heat pump heats and cools a building by exchanging heat with the outside air.

<u>AFUE</u> – Acronym for Annual Fuel Utilization Efficiency, a measure used to define the efficiency of a gas furnace. The higher the AFUE, the more efficient the system will be.

<u>ASHRAE</u> – Acronym for American Society of Heating, Refrigerating and Air-Conditioning Engineers. ASHRAE is a professional society for energy and mechanical engineers, contractors, and related disciplines. They produce the ASHRAE Standard 90.1 that is one of the most widely adopted standards for energy efficiency in buildings and is the backdrop for this study.

<u>Btu</u> – Acronym for British Thermal Unit, a unit typically used to define the size of heating and cooling loads and the capacity of HVAC equipment. Trade contractors, manufacturers, and designers often use Btu to define the size of a heating or cooling system (e.g., a 24,000 Btu air conditioner).

<u>Cavity insulation</u> – In light framed construction, building walls are constructed of 2x4 or larger studs spaced 16 or 24 inches apart. The space between the studs is called the cavity. Typically, fiberglass, cellulose, mineral wool, or some other type of insulation is installed in the cavity, hence the term "cavity insulation."

<u>CFL</u> - Acronym for compact fluorescent light. In layman's terms, CFLs are long lasting, highly efficient light bulbs that can be used in many fixtures that take an incandescent bulb.

<u>Continuous insulation</u> – Continuous insulation typically goes on the outside of a wall as opposed to inside the wall framing cavity. In this report and in many codes and standards, when both cavity and continuous insulation is required, the cavity R-Value is expressed first followed by the R-Value of the continuous insulation. For example, R21+5 would indicate that R-21 insulation is required in the cavity in addition to R-5 on the exterior of the studs. Continuous insulation is typically a foam-based product.

<u>COP</u> - Acronym for Coefficient of Performance. COP is typically used to describe the efficiency of a heat pump and refrigeration systems. In this report, COP is used to express the efficiency of a ground source heat pump in the heating mode. The higher the COP, the more efficient the system will be.

<u>EER</u> - Acronym for Energy Efficient Ratio, a term used to define the efficiency of a cooling system. In this report, EER is used to define the efficiency of a ground source

heat pump in the cooling mode. The higher the EER, the more efficient the system will be.

<u>Envelope (thermal)</u> – The insulation in a building is designed to separate the inside, conditioned space from outside conditions. This physical separation is often called the thermal envelope. Items outside the thermal envelope, such as in an attic, are considered to be outside the conditioned space of the building.

<u>GSHP</u> - Acronym for Ground Source Heat Pump. Also called a geothermal heat pump because heat is exchanged with the earth through a well, surface water, or underground loop to provide heating, cooling, and water heating for a building. This differs from the typical air-source heat pump which exchanges heat with outside air. A GSHP is generally much more efficient than other HVAC systems.

<u>HSPF</u> - Acronym for Heating Seasonal Performance Factor. HSPF is used to define the efficiency of a heat pump in the heating mode. The higher the HSPF, the more efficient the system will be.

<u>HVAC</u> - Acronym for Heating, Ventilating, and Air-Conditioning. Even when there is no mechanical ventilation component, it is not uncommon for a heating or cooling system in a building to be called an HVAC system.

<u>IECC</u> - Acronym for International Energy Conservation Code, published by the International Code Council. The IECC is the most widely used energy efficiency code for buildings in the United States. It adopts by reference the ASHRAE 90.1 standard.

<u>NFRC</u> – National Fenestration Rating Council. NFRC is generally recognized as the authoritative source for information on the thermal performance of windows. They maintain a listing of certified products which was used as a resource for this study.

<u>Performance requirements</u> – Building codes and standards often contain both performance and prescriptive requirements. A performance requirement tends to specify a result and lets the user determine how to achieve it.

<u>Prescriptive requirements</u> - A prescriptive requirement in a code or standard is very specific in explaining what exactly is required at the component level. For example, a code may have specific R-Values for wall or attic insulation. This is in contrast to a performance requirement that typically allow for numerous ways to comply.

<u>PV</u> - Acronym for photo-voltaic. PV is a technology that is used to generate electricity using energy from the sun. PV panels can be used on the roofs of buildings to minimize or offset the amount of electricity needed from the utility provider. It is also frequently referred to as "solar-electric."

<u>Reference Design</u> – Performance options in codes allow a designer to evaluate the overall performance of a building against a specific standard using an energy simulation

software program. The standard that a proposed design is compared against is called the reference design.

<u>R-Value</u> – A measure of the resistance of a building component to the flow of heat. R-Value is the inverse of the thermal conductance, or U-Factor. Insulation levels in a building are typically defined as an R-Value. The higher the R-Value, the better the wall or other building component is at slowing heat loss.

<u>SEER</u> - Acronym for Seasonal Energy Efficiency Rating used to measure the efficiency of an air-conditioning system. The higher the SEER, the more efficient the system will be.

<u>SHGC</u> - Acronym for Solar Heat Gain Coefficient. SHGC is a measure of the ability of a windows and other glazing to block solar radiation. In most cases, the lower the SHGC, the better the window will be from an energy efficiency standpoint.

<u>U-Factor</u> - A measure of the thermal conductance of a building component. U-Factor is the inverse of the R-value. The lower the U-factor of a window, wall, or other assembly, the more efficient it will be.

#### PROJECT BACKGROUND

#### Rationale for the Study

The American Society of Heating, Refrigerating and Air-Conditioning Engineers (ASHRAE) and the U.S. Department of Energy (DOE) recently announced a cooperative program to significantly increase the efficiency requirements for buildings. In a July 30, 2007 release, the organizations announced a goal of a 30% increase over today's standards by 2010 (www.ashrae.org/pressroom/detail/16399). This dovetails

with legislation before Congress in 2007 that would have required DOE to develop Federal standards if building and energy codes did not increase their efficiency requirements. Performance increases as high as 50% over today's codes by 2020 were addressed in the legislation. Although these parts of the legislation were ultimately removed in House-Senate conference negotiations as part of the Energy Independence and Security Act, proponents have made it a priority to bring them before Congress again.

This new initiative provides an opportunity for ASHRAE and DOE to expand our collective energy conservation efforts, our energy conservation education initiatives and strategic research program focus in leading our country and the world toward a sustainable energy future

- Kent Peterson, ASHRAE president in news release announcing a goal of 30% improvement in ASHRAE energy efficiency standards by 2010.

The feasibility of such increased building performance requirements and their impact on building costs are important issues that need to be understood. This study provides one of the few detailed looks at the costs and feasibility of large increases in energy efficiency for apartments and similar multi-family buildings. The results are intended to assist legislators, codes and standards developers, and other policy makers in addressing energy efficiency in multi-family buildings in a balanced and informed manner.

# Multi-family Housing – A Unique and Efficient Form of Housing

The impact on building costs due to increased regulations is an important issue for owners, developers, builders, and renters of all buildings, but apartments and other multi-family buildings in particular. One-size-fits-all goals for energy efficiency improvements can lead to consequences that were never intended. Considering that newer multi-family buildings are often the most sustainable form of housing – due to their higher density, lower material use per unit, and inherently lower utility costs – it is particularly important that society carefully weigh the impacts of how and whether to layer additional regulatory requirements on this important part of the housing market. Sustainable policies should encourage already efficient types of construction and be carefully evaluated so as to not discourage their selection by developers.

#### Regulating Building Energy Efficiency through Codes and Standards

There are a wide variety of ways in which energy efficiency is regulated in the United States. Although manufactured homes are regulated under a Federal standard administered by the U.S. Department of Housing and Urban Development, almost all other buildings are regulated by state or local governments.

Some states like California have developed their own energy efficiency codes geared to specific needs of the state. At the other extreme, some states have no requirements at all, or limit them to only certain types of buildings. Within these states, local communities may adopt their own codes and standards. Adoption of a model code or standard developed by a third party is the primary way local communities and states create their building code regulations.

The two most widely recognized third-party energy documents adopted by state or local jurisdictions are the ASHRAE Standard 90.1 (*Energy Standards for Buildings Except Low-Rise Residential Buildings*) and the International Energy Conservation Code (IECC).

ASHRAE 90.1 has a scope that covers all buildings except single-family and other low-rise residential buildings, whereas the IECC covers all types of buildings. The 2006 IECC and 2004 90.1 standard each have multiple options for compliance.

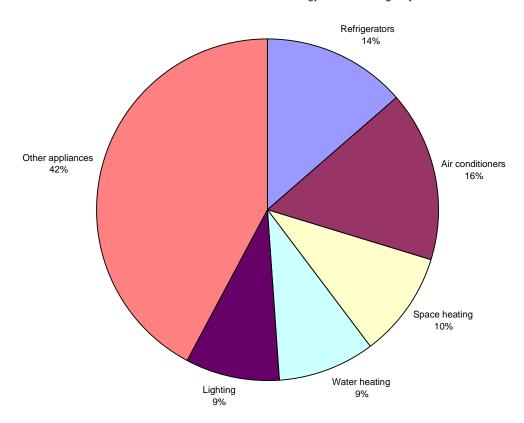
Interestingly, one compliance option within the IECC is to comply with the requirements of ASHRAE 90.1. Thus, many people believe that the IECC and 90.1 provisions result in a similar level of performance. Technically, they do have significant differences.

Perhaps more important than the differences between the IECC and 90.1 are those items not regulated by either document. These include energy use related to TVs, radios, office equipment, computers, and other plug or miscellaneous loads; refrigerators, washers, dryers, and other large appliances; and portable lighting within dwellings. Both documents also only indirectly address the heating and cooling energy related to air infiltration.

The electrical energy related to various end uses in a residential building is shown in Figure 1. Refrigerators, other appliances, and lighting represent 65% of the electrical energy in a residential building even though these end uses are not regulated directly by 90.1 or the IECC for dwelling units.

Figure 1 – Residential electricity by end use (2001)

Source: US. Energy Information Agency RECS data



It is important that policy makers realize that a 30% or 50% increase in code requirements will not result in an equivalent decrease in whole-building energy consumption. On the other hand, there will be extreme practical and economic limitations that should be considered if end uses that, for example, only amount to 35% of the energy in an all electric building must shoulder a 30% or 50% reduction for the entire building.

# ASHRAE 90.1 versus the International Energy Conservation Code

ASHRAE Standard 90.1 has a scope that covers all buildings except single-family and other low-rise residential buildings. These smaller residential building types are covered under a separate ASHRAE standard.

The IECC scope includes all types of buildings, although residential requirements are contained within a separate chapter than other buildings. The 2004 IECC has multiple options for compliance of large residential and commercial buildings, one of which is meeting the requirements of ASHRAE 90.1. The IECC also has its own prescriptive and performance options for compliance.

The IECC performance approach requires the same simulation tool be used for the proposed design and the reference design but otherwise provides little additional information on how to select a simulation tool. On the other hand in ASHRAE 90.1, the standard specifies explicit criteria for how to use the performance (modeling) approach (e.g., the model must be an hourly simulation tool) and gives examples of acceptable modeling tools including BLAST and DOE2. Both documents require input and output files as documentation for the simulations.

The 90.1 performance method is called the "energy cost budget" method. Table 11.3.1 of the standard provides specific instructions for how to model the proposed design and the reference design under this approach. Unfortunately, the energy cost budget method tends to restrict the scope of areas where a designer could make more energy efficient selections for a building. For example, individual domestic water heaters within apartments must be identical in the reference design and proposed design, effectively taking this significant item off the table in terms of reaching the proposed goals of 30 or 50% better than 90.1. Lighting inside dwellings and infiltration are other similar examples.

The energy simulation software we used to develop the cost budget method in this study calculates a report that shows the overall energy costs for all energy uses covered by 90.1. To perform this analysis, location-specific fuel costs are required as inputs. It also shows the energy use associated with the building and breaks this item and the costs into the following components: Total electricity, area lights, miscellaneous electric loads, pumps, space cooling, space heating, vent fans, total natural gas, and space heating for gas. Note that no water heating costs are reported, although water heaters must be input since they must still meet the minimum prescriptive efficiency requirements.

#### Use of Standard 90.1 over IECC for this Study

In performing this analysis of what it takes to reach "better-than-code" efficiency targets, we based our study on the ASHRAE 90.1 requirements over the IECC for three main reasons:

- 1. The two documents are often considered equivalent standards, but the IECC offers one compliance path that requires meeting the 90.1 requirements. Thus, complying with 90.1 technically results in compliance with both documents.
- 2. There are no recognized simulation tools that automatically develop a reference design for an apartment building under the IECC, whereas there is a respected modeling tool that does so for 90.1. This takes some of the user bias out of the process that can be introduced with tools that require the user to develop the reference design themselves.
- 3. ASHRAE requirements often are used as the basis for requirements in other codes. Further ASHRAE has already initiated efforts to increase their

performance levels by 30% in the next edition of 90.1. Thus, the impact of more stringent requirements may be more time sensitive for 90.1 than the IECC.

Note that when we refer to ASHRAE 90.1 throughout this document, we are discussing the 2004 edition unless otherwise indicated.

#### STUDY METHODOLOGY

A computer simulation offers the most direct method for comparing how a proposed design compares to the 90.1 standard or the IECC. For this study, we selected three cities that have relatively large numbers of apartments built each year and that are located in very different climate zones. The simulations were run on a four-story apartment building in each climate location using the energy cost budget method described in Chapter 11 of ASHRAE 90.1 (2004 edition). The four-story building prototype was based on typical multi-family designs being constructed in the market today, based on dialogue with industry experts.

The energy cost budget method is frequently used by designers to establish compliance or to see how their design otherwise compares to 90.1. Although our study was based heavily on results of simulations following the energy cost budget method in the 2004 edition of ASHRAE 90.1, where appropriate, we used other estimation methods to address unique situations.

In addition to the computer simulations, we also conducted the following activities:

- 1. Developed cost estimates of the options necessary to achieve energy performance of 15%, 30% and 50% above ASHRAE 90.1.
- 2. Described any obstacles to the 15%, 30% and 50% thresholds including technical barriers, problems with product availability.
- 3. Provided guidance or comments on how the feasibility of achieving energy performance 15%, 30% and 50% above 90.1 might improve in the future or under different scenarios.

There are dozens of simulation tools available to assess a building's performance. We chose Energy Gauge Premier Summit (V.3.11) for this study. Energy Gauge (EG) is maintained by the Florida Solar Energy Center at the University of Central Florida. The rationale for selecting EG and its advantages and limitations are provided in Appendix A.

#### **Assumptions**

Assumptions for the study are addressed in the following sections:

#### **Locations**

We selected Atlanta, Chicago and Houston as the locations. These cities gave us a mix of climates including cooling dominated (Houston: 90.1 Climate Zone 2), heating dominated (Chicago: Climate Zone 5) and a mixed climate (Atlanta: Climate Zone 3). We also were able to look at different fuels for heating since the norm for apartments in Houston and Atlanta is an electric heat pump but it is a gas furnace in Chicago.

#### **Fuel Costs**

Fuel costs assumed for each location are shown in Table 1. Within each location, there are generally several options a consumer can select for their rates. We chose the flat rate plan for each location. Rates are those in place as of October 2007.

Table 1 – Electricity and natural gas charges

Location	Electric use and distribution rate (\$/kWh)	Electric monthly account fee (\$/month)	Natural Gas use and distribution rate (\$/therm)	Natural Gas monthly account fee (\$/month)
Atlanta	0.0783	7.50	0.999	8.99
Chicago	0.0766	6.69	1.23	8.99
Houston	0.15	none	0.967	10.50

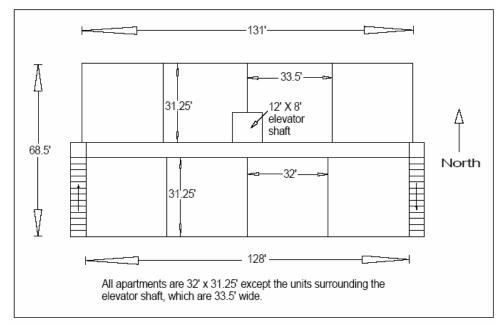
#### **Building Characteristics**

There are many different types and sizes of apartments and multi-family buildings, making it difficult to determine the impact of energy efficiency standards on these building as a whole. We selected an apartment building with components designed to meet the minimum prescriptive requirements of 90.1. In other words, we started with typical materials and systems used for low-rise (four-story or less) apartment buildings and selected prescriptive minimums for each thermal component.

The base building is a four -story apartment with eight units per floor of roughly 1000 square feet each. The building has a slab foundation and a 6/12 pitch gable end roof with an unconditioned attic. All duct work and equipment was assumed to be in conditioned space. Each apartment unit was assumed to have an individual heating, cooling, and hot water system serving only that specific unit, all typical practices in the apartment market.

Other characteristics of the base building are shown in Table 2 and Figure 2 below.

Figure 2- Sketch of floor plan of apartment building (all floors are identical)



#### **Table 2– Building characteristics**

#### General size/shape characteristics

- Four-story building
- Type V (wood) framing
- 8 units per story
- One bedroom units
- Approximately 1000 sf per unit
- 8' ceiling height
- Exits from units are direct to common center corridor within the thermal envelope.
- Elevator located in center of corridor within thermal envelope.
- Building exit stairs are outside of the conditioned space (open to outside air)
- Long dimension runs east to west (most windows on the north and south sides)
- Roof framing materials are wood trusses on a 6/12 pitch.
- Walls are wood stud with vinyl siding
- Foundation type: Slab on grade in all locations

#### **Equipment**

- Individual water heaters in each unit meeting 90.1 minimum efficiency requirements (40 gallon tank type, gas)
- Individual HVAC units with minimum 90.1 efficiency in each dwelling
  - SEER 12 heat pumps in Atlanta and Houston
  - o 80 AFUE gas furnace with separate SEER 12 AC in Chicago
- Through the wall ductless SEER 10 units in corridors
- All equipment, supply and return ducts are inside the conditioned envelope

Thermal envelope properties'			
	Atlanta	Chicago	Houston
Roof insulation: minimum prescriptive R Value	R-38	R-38	R-38
Exterior door: Steel with minimum R value	R-2.6	R-2.6	R-2.6
Wall framing: minimum prescriptive R Value	R-13	R-13	R-13
Window type: double hung, operable with closest values as is commercially available that are under the maximum code prescriptive SHGC and U values (from NFRC listings)	SHGC and U vary by climate and orientation  – see inputs in appendix for specific window properties		
Average window to wall ratio (expressed as percentage)	About 23% of gross wall area (these vary by wall, see the input files in appendix for specific areas)		
Unit separation walls: Wood frame (Note: not significant since all adjacent to conditioned space)	R-13	R-13	R-13
Raised floors: Wood frame (Note: not significant since all adjacent to conditioned space)	R-19	R-19	R-19
Infiltration	ASHRAE crack method for proposed and reference design. (not governed by 90.1 except in prescriptive option)		

#### Thermal zones for building simulations

- Dwelling units: 18 conditioned zones arranged so that only units with the same orientation and exposure conditions were grouped
- Corridors: 3 conditioned zones (4th floor, 1st floor, combined 2<sup>nd</sup> and 3<sup>rd</sup> floor zone)
- Attic: One unconditioned zone
- Elevator: One unconditioned zone but located entirely within other conditioned space.
- Stairways: Not included as zones since outside of the thermal envelope

<sup>&</sup>lt;sup>1</sup> U values corresponding to these R-values were selected from the 2004 ASHRAE 90.1 Normative Appendices for all components exposed to unconditioned space, except where not covered in the normative appendices. For example, an R-40 was used for a SIPS panel since wall framing in the normative appendices is based on stud wall assemblies.

#### SIMULATION RESULTS

#### **Review of Energy Upgrades and Resultant Savings**

The simulation results are the focus of this study because they identify the options that can most help a designer reach a certain goal above the 2004 ASHRAE 90.1. Table 3 shows the outputs for the design of the base buildings in Atlanta, Chicago, and Houston. The 90.1 reference costs in the table are automatically generated by Energy Gauge to represent the energy cost budget that is required for compliance with 90.1.

Table 3 – Base annual building energy cost budget simulation results

Simulation results				
	Atlanta	Chicago	Houston	
	90.1	90.1	90.1	
	reference	reference	reference	
Total Cost Budget	\$32,946	\$56,951	\$64,960	
Electricity	\$32,946	\$25,323	\$64,960	
Area lights	\$6,895	\$6,746	\$13,175	
Misc. Equipment	\$4,733	\$4,630	\$9,044	
Pumps & Misc.	\$39	\$836	\$67	
Space cool	\$4,491	\$2,078	\$18,733	
Space heat	\$8,781	\$2,653	\$8,138	
Vent fans	\$8,007	\$8,380	\$15,804	
Natural gas		\$31,628		
Space heat		\$31,628		

The 90.1 reference costs for each location represent the metric against which changes to the building were evaluated in later simulations. In other words, as changes were made to upgrade a component in the base building (for example, increasing attic insulation), a new proposed design energy cost budget was developed. The total energy cost associated with the building was compared to the reference total costs in Table 3 to derive a percentage better than the 90.1 reference. Thus, a building with a proposed design energy cost budget of \$90,000 would be 10% better than a reference design with an energy cost budget of \$100,000.

As mentioned earlier, the outputs and input files are required by 90.1 to support use of the energy cost budget method. Because each input file is more than 20 pages in length, for practical purposes we have only included the input reports for the three base buildings in Appendix B of this report. For subsequent simulations, summary tables showing the results indicate what items were modified in the inputs.

Initially, only individual components were changed and all other inputs to the building were held constant. We then went on to evaluate combinations of improvements to see what was necessary to reach the 15%, 30%, and 50% levels of improvement above ASHRAE 90.1.

Results of the simulations are shown in Tables 4 to 6. Everything in the baseline building was held constant except for the items in the far left column of the tables. As

an example, the entry "R-49 attic" indicates that the baseline building attic insulation was increased to R-49. Likewise, "R-49 attic, R-19 wall" indicates that the attic insulation was increased to R-49 and the exterior wall insulation was increased to R-19, but all other inputs are as defined in the baseline building characteristics in Table 2 and the input files in Appendix B were unchanged. Where required by the standard, R-values were selected to be equivalent to the inverse of the U-Factors as described in the 90.1 Normative Appendices.

Over 110 simulations were run in the three locations. Not all of the results are shown in Tables 4, 5, and 6, nor are all of the options shown identical for each city. Generally, items that made little difference in the energy cost budget were omitted unless they were related to the envelope R-Values. We specifically included R-Value improvements even if they had little improvement because these are the items that are most often thought to provide meaningful improvement to a building's performance.

Table 4 - Atlanta Simulations

<b>Description</b> (items in parenthesis are the <u>baseline</u> building characteristics for the item or items that were changed for each simulation)*	% of 90.1 Reference Building	% Better than Reference Building
Baseline building	100	
Doors R-5.2 (R-2.6)	99.88	0.12
R-49 attic (R-38)	99.85	0.15
R-19 walls (R-13)	99.56	0.44
U=0.3, SHGC=0.19 *	99.39	0.61
R-21+5 walls (R-13)	99.12	0.88
R-49 attic, R-21+5 walls (R-38,R-13)	99.08	0.92
R-5 subslab (R-0)	99.01	0.99
R-40 walls (R-13)	98.72	1.28
R-49 attic, R-40 walls (R-38,R-13)	98.67	1.33
R-49 attic, R-40 walls, R-5 under slab (R-38,R-13, R-0)	97.55	2.45
SEER 15/HSPF 8.3 Heat pump (SEER 12/HSPF 7.4)	95.60	4.40
SEER 19,/HSPF 10 Heat pump (SEER 12/HSPF 7.4)	90.42	9.58
SEER 19,/HSPF 10 Heat pump, R-49 attic, R-21+5 walls, U=0.3, SHGC=0.19 (SEER 12/HSPF 7.4, R-38, R-13) *	89.25	10.75
SEER 19,/HSPF 10 Heat pump, R-49 attic, R-21+5 walls, R-5.2 door, U=0.3, SHGC=0.19 (SEER 12/HSPF 7.4, R-38, R-13, R-2.6)	89.15	10.85
SEER 19,/HSPF 10 Heat pump, R-5 subslab, R-21+5	88.90	11.10
SEER 19,/HSPF 10 Heat pump, R-49, R-21+5, R-5.2 door, R-5 subslab, U=0.3, SHGC=0.19 , (SEER 12/HSPF7.4, R-38, R-13, R-2.6, R-0) *	88.26	11.74
GSHP (3.7 COP, 16.9 EER) (SEER 12/HSPF 7.4)	68.85	31.15
GSHP, R-49attic, R-21+5 walls, , R-5.2 door, R-5 subslab, , U=0.3, SHGC=0.19 (SEER 12/HSPF 7.4, R-38, R-13, R-2.6, R-0) *	60.62	39.38

<sup>\*</sup> Windows in the baseline building vary by wall orientation. See Appendix B for specific values.

Some options made significant differences in one climate but not necessarily in all climates (e.g., subslab insulation). Many different variations of shading and window

orientation also are not shown because they contributed little to no improvement in the building's overall performance. Lighting variations were simulated because lights represent a significant potential for energy savings. However, lighting was omitted from tables 4, 5 and 6 because it is an item that cannot be used to improve compliance within dwellings in 90.1. Lighting is discussed in a different context in the next section (Opportunities with 90.1 scope changes) since it does represent a large potential opportunity if 90.1 were restructured.

**Table 5 - Chicago Simulations** 

Description (items in parenthesis are the baseline building characteristics for the item or items that were changed for each simulation)	% of 90.1 Reference Building	% Better than Reference Building
Baseline building	92.52	7.48
R-5.2 alum/poly door (R-2.6)	92.51	7.49
R-49 attic(R-38)	92.32	7.68
R-19 wall (R-13)	91.71	8.29
R-21+5 walls (R-13)	90.89	9.11
R-49 attic, R-21+5 walls (R-38, R-13)	90.68	9.32
R-21+10 walls (R-13)	90.55	9.45
R-40 Walls (R-13)	90.12	9.88
R-49 attic, R-40 walls (R-38, R-13)	89.92	10.08
R-5 subslab (R-0)	89.10	10.90
96 AFUE Furnace (78 AFUE)	84.81	15.19
96 AFUE furnace, SEER 19 AC (78 AFUE, SEER 12)	83.94	16.06
R-49 attic, R-40 walls, 96 AFUE furnace, SEER 19 AC, R-5 subslab (R-38, R-13, 78 AFUE, SEER 12, R-0)	78.78	21.22
3.7 COP/16.9 EER GSHP (78 AFUE furnace + 12 SEER AC)	54.96	37.15
3.7 COP/16.9 EER GSHP, R-49 attic, R-40 walls, R-5 subslab (78 AFUE furnace + 12 SEER AC, R-38, R-13, R-0)	47.93	46.07

**Table 6 - Houston Simulations** 

<b>Description</b> (items in parenthesis are the baseline building characteristics for the item or items that were changed for each simulation) *	% of 90.1 Reference Building	% Better than Reference Building
Baseline building	93.51	6.49
R-5.2 alum/poly door (R-2.6)	93.43	6.57
R-49 attic (R-38)	93.41	6.59
32 inch shading N side (none)	93.34	6.66
32 inch shading SEW sides (none)	93.28	6.72
R-19 wall (R-13)	93.19	6.81
32 inch shading all sides (none)	93.11	6.89
R-21+5 walls (r-13)	92.85	7.15
R-49 attic, R-21+5 walls (R-38, R-13)	92.75	7.25
R-21+10 walls (R-13)	92.71	7.29
R-40 Walls (R-13)	92.54	7.46
R-49 attic, R-40 walls (R-38, R-13)	92.44	7.56
U=0.3, SHGC=0.19*	92.38	7.62
SEER 15/HSPF 8.3 Heat pump (SEER 12/HSPF 7.4)	86.52	13.48
SEER 15 HP/8.3 HSPF Heat pump, R-40 walls, R-49 attic, U=0.3, SHGC=0.19 (SEER 12/HSPF 7.4, R-13, R-38)*	84.76	15.24
SEER 19/HSPF 10 Heat pump	83.99	16.01
SEER 19/HSPF 10 Heat pump, R-40 walls, R-49 attic, U=0.3, SHGC=0.19 (SEER 12/HSPF 7.4, R13, R-38)*	80.49	19.51
3.1 COP/14.6 EER GSHP (SEER 12/HSPF 7.4)	59.23	40.77
3.1 COP/14.6 EER GSHP, R-40 walls, R-49 attic, U=0.3, SHGC=0.19 (SEER 12/HSPF 7.4, R-13, R-38)*	52.39	47.61

<sup>\*</sup> Windows in the baseline building vary by wall orientation. See Appendix B for specific values.

The table entries are shown to the second significant digit. This does not imply that the simulations are that precise. Typically, we would round the numbers to the nearest whole number. The digits to the right of the decimal point are shown only to illustrate just how small the associated impact is due to some of the items that are typically thought to contribute significantly to improved performance.

As shown in the tables, obtaining performance levels of 15% above 90.1 in Chicago and Houston would require a combination of improvements to the envelope and higher efficiency equipment. In fact, one could reach the 15% level without changes to the envelope by simply selecting high efficiency equipment (e.g., jumping to a SEER 19 heat pump in Houston).

The methods, materials and equipment to reach 15% in Chicago and Houston would fall within the range of what we might call normal upgrades to a building. The biggest barrier to this level of performance is generally higher first costs, rather than any type of technological feasibility issue.

Reaching the 30% and 50% threshold in Houston and Chicago, and the 15% threshold in Atlanta, would require a jump to what we might call extraordinary equipment or

practices, and/or changes to the 90.1 scope. For example, the equipment efficiency that would be required to reach these levels would generally require ground source heat pumps (GSHP) or similar advanced technology. Higher end air source heat pumps or other conventional equipment that is currently commercially available is not efficient enough to reach these goals, even when combined with extensive envelope improvements. In the three climates examined, even very advanced equipment would be unlikely to achieve the 50% goal for an apartment building. The scope of 90.1 would need to change to recognize lighting, water heating energy, and onsite renewable energy production (e.g., PV or wind) as an allowable method to offset building energy use in the energy cost budget method.

# The Baseline Building Compared to the Reference Building

Except for the Atlanta results in Table 4, the reader should not interpret that a specific option or group of options is solely responsible for the improvement over the 90.1 reference shown in the far right column of the Tables 4 to 6. The actual contribution of an option is the difference between the far right column and the baseline buildings "% of 90.1 reference building" in the center column. For example, the use of R-49 attic insulation in Houston (Table 6) would result in a 0.10% improvement over the baseline building. In Houston, the baseline building designed to 90.1 prescriptive minimums (or in the case of windows, the nearest commercially available window to the minimum) already performed better than the reference design by 6.49%. Thus increasing attic insulation from R-38 to R-49 yields a 0.10% improvement (93.51% versus 93.41%).

This also helps explain why it was more difficult to reach the 15% goal in Atlanta without resorting to extraordinary equipment as opposed to the other locations. The baseline building in Atlanta, designed to 90.1 prescriptive minimums, was at about 100% of the reference design energy cost budget. Thus, in Atlanta, the building did not have the same "head start" as Chicago and Houston where the minimum prescriptive requirements resulted in a building that was already 6.5% to 7.5% under the reference energy cost budget.

#### **Energy Savings from Envelope Improvements**

Since opaque envelope improvements are typically the first items targeted for code changes, it is important to understand how they could impact the performance of a building. Figure 3 illustrates selected envelope improvements from the simulations in Atlanta. Note that most envelope improvement by themselves provided less than 1% energy savings. Even combining multiple improvements offered less than a total of 2.5% improvement. Similar results were found in Chicago and Houston. The only exception seems to be the addition of R-5 subslab insulation in Chicago, which produced about a 3-1/2% savings over R-0 subslab insulation.

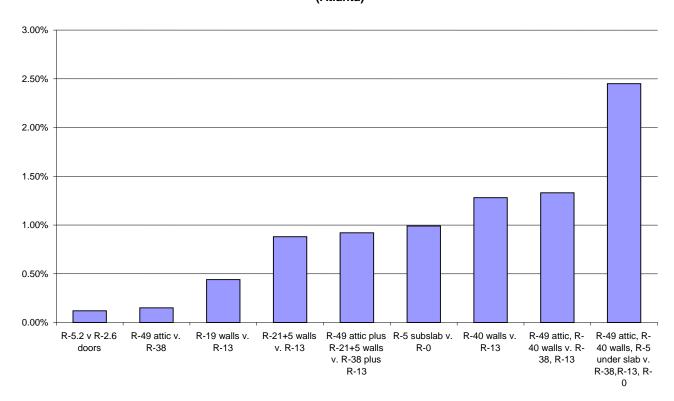


Figure 3 - Improvement due to selected component changes over base building (Atlanta)

It is not possible to save the same energy multiple times so the reader is also cautioned against adding the results of different simulations. The impact of any two or more individual options is not always additive because the options tend to interact with each other. Thus, only when multiple options are input simultaneously in a simulation do the results reflect their combined contribution.

Further discussion of the simulation results is provided in a later section of this report. However, we would caution that results from this study should not be taken as definitive measures of how the options we simulated will impact every building. All buildings are unique. Utility rates vary by location. Likewise, different simulation tools or estimating methods would likely yield different results for a similar building. Thus percentage of improvements should not be taken as firm indicators in every situation. Rather they illustrate the likely range of improvements with different design options.

In addition, we found it necessary to apply some judgment and other estimation tools for some system options. These impacted the way we addressed GSHPs and lighting. Details of these analysis steps are presented in Appendix D.

#### **Unexpected Outcomes**

Not all of the simulations provided outcomes that were intuitive. We were surprised by at least a few. These are addressed in the following paragraphs.

Advanced windows and shading provided little benefit. Designers have been taught for decades that thermal characteristics, shading and orientation of windows are critical factors in energy efficiency. A common rule of thumb in cold climates is to use adequate windows on the south-facing orientation for winter heat gain while providing sufficient shading to minimize heat gain in the summer. Also, the lower the U Factor and SHGC, the better in cooling-dominated climates.

So why did the simulations show that window characteristic did not add all that much to the building's overall performance? There are several possible answers. One is that apartment buildings like the one we simulated have a small amount of window area compared to floor area relative to single-family homes and other buildings. A second is that the baseline windows that we used are already fairly good performers. Minimum requirements in codes and standards have pushed up the quality of windows over the years. Thus the combination of better baseline windows and small relative window area would already "use up" some of the improvements we would have expected when we went to a better window.

To test our theory on why windows did not have as much impact as we expected, we ran additional simulations on the Houston building with windows having relatively poor thermal performance. In this case, we assumed a U=0.9 and a SHGC=0.73. This would roughly correlate to a double pane metal window or a single pane wood window.

The building with the "poor" performing window was compared to the advanced windows (U=0.3, SHGC=0.19) to show the potential range of improvement. Whereas the advanced windows generally provided about 0.5% improvement over the baseline windows, the advanced windows provided a 3.5% difference in the 90.1 energy costs compared to the poor performing window. This equates to about 5.4% of the heating and cooling energy costs, which is more in line with our initial expectations and conventional thinking on this subject.

Insulation on ducts did not improve the building's performance: Adding R-8 insulation to the ducts did not show any improvement relative to the baseline building we simulated. Typically, duct losses are understood to contribute a significant amount to the energy use in a building. However, in the case of newer apartment buildings, ducts are typically inside the conditioned space. We thus also assumed ductwork within the conditioned space for the simulations. Once inside conditioned space, the addition of insulation would not be expected to improve the building's energy performance, although there are other benefits attributable to insulating these ducts.

Subslab insulation was not very effective in Atlanta and showed no benefit in Houston: We expected that subslab insulation might have more of an impact in Atlanta because it

has a significant heating load and that it would have at least some impact in Houston. One explanation for the results is that complete coverage of the subslab area "blocks" "free cooling" from the soil. Thus, the net heat gain for the building rises in the cooling season more than the heat loss that is reduced in the heating season. In a colder climate like Chicago the subslab insulation would be much more effective than in a cooling-dominated climate like Houston, or a mixed climate like Atlanta where there are significant heating and cooling seasons.

#### **OPPORTUNITIES WITH 90.1 SCOPE CHANGES**

Results of the simulations show the difficulty that designers may face in reaching levels of 30% and 50% above ASHRAE 90.1. However, there may be some changes to 90.1 - specifically in broadening the scope of the standard to include items that are currently not part of the energy cost budget method - that could help a designer reach these levels of performance. This section discusses the major opportunities that could help make the 30% and 50% thresholds more obtainable.

#### **Water Heaters**

In Table 11.3.1 of 90.1, individual domestic water heaters in dwellings are effectively excluded from the cost budget method since the same system and characteristics must be applied to the design and reference buildings. The lone exception is where a boiler provides space heating and water heating. Water heaters are relegated to a pass/fail test for compliance based on the unit efficiency compared to the 90.1 minimum. This is also the method used in the IECC performance approach for commercial (including multi-family) buildings. Interestingly, the IECC performance approach for single-family homes *does* allow the designer to take credit for more efficient water heating equipment.

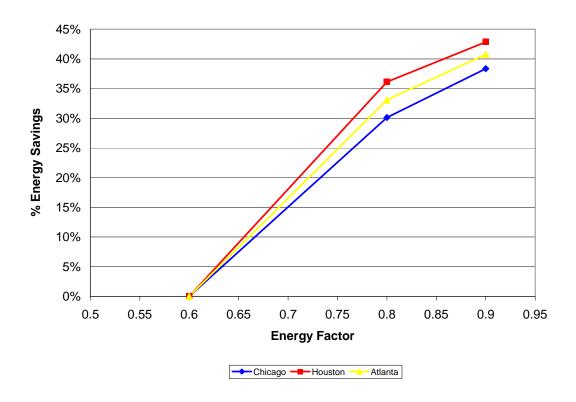
There may be good reason to explain why 90.1 does not recognize energy savings due to increased water heater efficiency in the energy cost budget method. It may be that water use in a building varies so much that the developers of 90.1 did not want to give credit to a design that could result in a broad range of savings in buildings. However, even when taking into account the variability and making conservative assumptions on water use patterns, there is a considerable amount of potential savings related to selection of more-efficient water heaters. Perhaps the 90.1 committee reasoned that a residential water heater is not a permanent part of a building and could be replaced with less efficient equipment in the future.

Figure 4 shows the percent increase in energy savings that higher efficiency water heating equipment could achieve in the three climates we examined, relative to the 0.6 minimum efficiency specified in 90.1. In terms of energy costs, the 0.9 efficiency (expressed as EF or energy factor) equipment in the chart could save approximately \$1500 annually in Atlanta and Houston and about \$2200 in Chicago in the baseline

building. This translates into about a 4.5% reduction in the baseline energy cost budget for the buildings we modeled in Atlanta. A similar savings would be seen in Chicago and about 2.3% in Houston. The potential savings with water heating is much more significant than the changes to the building envelope.

Figure 4 – Performance of Water Heaters at Various Efficiencies relative to a 0.6 EF unit

Water Heater Savings Versus Efficiency in a 1 Bedroom Apartment



# Lighting

Section 9.1.1 (Scope) of 90.1 provides an exception for lighting inside dwellings from compliance with Chapter 9 requirements that govern lighting. Increasing the scope of 90.1 to include lighting inside dwelling units could help industry reach the 30% or 50% thresholds. A designer could specify high efficiency lighting fixtures and come in well below the lighting power allowance while still providing sufficient illumination for safety, task and general lighting.

The lighting power allowance for a dwelling in 90.1, which is expressed in Watts per square foot, appears to be generous for dwellings. It may be difficult for ASHRAE to lower the allowance in future editions of 90.1 without creating conflicts with corresponding lighting design standards, thus leaving significant opportunity to show savings under the 90.1 energy cost budget method.

Assuming that one could consider lighting in a better-than-code design effort, simply using CFL bulbs in all fixtures would enable a designer to improve upon the baseline building in Atlanta by just over 6%. As with water heater efficiency, improved lighting offers a much greater opportunity than envelope improvements and other more typical items governed by 90.1 and the IECC.

The downside to pursuing lighting in 90.1 is that expanding the scope of a standard always brings the risk of changes in the future that could be very difficult to exceed. From a long-term perspective, it could also be easy to replace CFLs with less efficient bulbs down the road, effectively negating the savings claimed during the design stage. Regulators may be tempted to require efficient fixtures rather than just bulbs to give them some assurance that the savings would be more permanent.

#### Renewable Energy

Renewable energy generated on-site is not permitted to be used to offset energy use in a building when evaluating designs according to the 90.1 energy cost budget method. However, if the goal of 50% is to be taken seriously, then this type of trade off may need to be considered by ASHRAE. In the three cities where buildings were simulated, we were unable to reach the 50% goal even with extremely high levels of insulation, top of the line windows and doors, and the most efficient HVAC technology.

Of the available options, PV (photo-voltaic or solar electric) is the renewable technology that would be most suitable and practical for a multi-family building, although it is not without limitations. Some of the issues that would need to be addressed include:

- Initial costs and on-going maintenance.
- Building orientation. This is perhaps the most important design consideration.
  The buildings in our simulations are ideally suited for PV because ½ of the roof
  surface faces due south. A designer would not always be able to take advantage
  of the orientation depending on a number of variables including but not limited to
  shape and size of the lot and building, shading, setbacks and other land use
  regulations.
- Available space on the roof. PV can be installed on exterior walls but it is much less efficient when installed vertically. For most buildings, available roof space probably will not be an issue to get to the 50% goal, assuming that significant HVAC equipment upgrades are also implemented. More important will be having enough roof space in the south-facing orientation.
- State regulations on net metering. Net metering policies at the state level are
  essential to the success of PV. Net metering allows a building owner to get
  credit on a utility bill for sending electricity back to the grid. This is the most
  efficient way to capture the energy that PV produces. Without net metering,
  prospects for efficient use of electricity generated by PV are severely limited,
  since the time frame when most electricity is generated from solar does not
  coincide with the peak demands in a dwelling.

Adjacent shading. On buildings in the inner city or where other higher buildings
effectively block the sun, PV is not very useful. Trees can also have the same
impact, but less so for a three or four-story building than for lower height
apartment buildings. Even partial shading can severely reduce the power
production from a PV panel.

The energy that would need to be supplied by PV to eliminate the gap between the highest performing options in the simulations and the 50% threshold is provided in Table 7. If as much as 25 kW of PV were needed on the roof, as is shown for Atlanta, about ½ of the south-facing roof space would be needed. If the building were oriented in a different direction, it might require significant changes to the roof shape and building design to provide the necessary space. Available roof area is very specific to a given building even though it happens to work out well for the buildings we studied.

Table 7 – PV requirements to meet the 50% threshold

Table 1 – 1 V requirements to meet the 30% threshold				
	90.1 reference costs			
	Atlanta	Chicago	Houston	
Total	\$32,946	\$56,951	\$64,960	
Electricity	\$32,946	\$25,323	\$64,960	
Natural gas (Space heat)		\$31,628		
% maximum savings w/o PV	39	46	48	
Max \$ savings w/o PV	\$12,848.94	\$26,197.46	\$31,180.80	
50% goal	\$16,473.0	\$28,475.5	\$32,480.0	
Amount to make up to get to 50%	\$3,624.06	\$2,278.04	\$1,299.20	
Electric rate (\$/kWh)	0.0783	\$0.0766	\$0.15	
PV energy required to reach goal				
(kWh)	46,284	29,739	8,661	
Expected energy production	4045	4045	4000	
(kWh/kW DC)	1345	1345	1222	
Derating factor	0.7	0.7	0.7	
Array tilt (degrees)	26.56	26.56	26.56	
Array Azimuth (degrees)	180	180	180	
PV array size needed (kW DC)	34.4	22.1	7.1	
Power density (W/sf)	10	10	10	
Panel area required (sf)	3441	2211	709	
Roof area available (sf)	4978	4978	4978	
Sufficient roof area to mount?	Yes	Yes	Yes	

#### Infiltration

Chapter 11 of 90.1, which addresses the energy cost budget method, does not directly address infiltration when there is no mechanical ventilation. One could logically assume that infiltration in the proposed design should be set equal to the reference building, since Section 11.3.2 (d) specifies that outdoor air ventilation rates should be equal in both buildings. This is consistent with the prescriptive requirements in 90.1 Section 5.4.3, which does not specify a minimum or maximum air change rate for buildings but instead requires envelope sealing at specific locations. The Energy Gauge developers interpret 90.1 in a manner consistent with our interpretation – they do not allow the user to input a different infiltration airflow rate for the reference or design buildings. Rather, they use the ASHRAE crack method to estimate the infiltration rate for both buildings.

Infiltration is a large component of the heating and cooling load of a building. ASHRAE's Handbook of Fundamentals (2001 edition, page 26.9) states that air exchange typically represents 20 to 50% of a building's thermal load. However, most data on infiltration has been limited to single-family buildings. The US EPA Energy star website claims 25 to 40% of energy used for heating and cooling is due to infiltration (<a href="http://www.energystar.gov/index.cfm?c=new\_homes\_features.hm\_f\_reduced\_air\_infiltration">http://www.energystar.gov/index.cfm?c=new\_homes\_features.hm\_f\_reduced\_air\_infiltration</a>) but it does not cite specific references for this range.

There is little information in the literature on larger buildings. A multi-family building may be more like an office building in regard to the impact of infiltration on loads. According to a study (Emmerich et. al., *Investigation of the impact of commercial building envelope air-tightness on HVAC energy use*, National Institute of Standards and Technology, 2005) of infiltration in office buildings, 33% of the heating load is due to infiltration in a typical building in the United States. The same study showed that infiltration may increase or decrease the cooling load, but on average increases it by about 3%.

Even if one takes a conservative estimate for amount of the thermal load due to infiltration, say 20%, this still represents a significant opportunity for ASHRAE to consider in 90.1. Of course, all of the infiltration load could not be accounted for in the cost budget method, nor should it. Some maximum level would need to be identified within the 90.1 standard and credit given for anything below the maximum. Otherwise, a designer could set an artificially high air infiltration rate and then get credit for reducing it without any intention of ever constructing the building with a tighter envelope. At some point, a lower threshold would also limit the credit one could receive toward compliance under the cost budget method, since mechanical ventilation would be necessary if the building were too tight. A maximum infiltration rate perhaps set to a regional average could be considered. Even within these limitations, even if only 5% of the infiltration load could be open for a credit toward compliance, this would represent an improvement of over 3% to 3-1/2% in the total energy cost budget of a 90.1 reference building in the three locations we examined. Again, this type of improvement would be much more significant than other changes to the building thermal envelope.

# **Plug Loads**

Miscellaneous electrical loads, mostly in the form of plug loads, are another potential area for ASHRAE to consider expanding the scope of 90.1 to cover. In the buildings we simulated, these loads accounted for about 14% of the 90.1 reference building's energy cost budget in Atlanta and Houston and about 8% in Chicago.

There are many potential problems that could arise if plug loads were to be part of the 90.1 scope for an apartment building. Perhaps most significant is that the developer or builder does not have control over occupants or how they use miscellaneous equipment, small appliances, and consumer electronics. Thus, even though there is a lot of energy at stake, regulating plug loads within 90.1 would likely prove difficult to implement.

## **Building Orientation**

The direction a facade faces, combined with the amount and type of glazing on the façade, influences the heating and cooling losses and gains in a building. In the northern hemisphere, it is generally understood that south-facing glazing helps with the heating of the building but can increase the cooling load.

Shading of windows helps to reduce the impact on cooling and allows the winter sun, which is lower in the sky, to provide heat in the winter. However, simulations conducted with shading did not show much impact on the building performance. Improving the windows also did not improve the overall building very much. Some of the low performance illustrated with shading and higher performance windows could be attributed to the fact that the baseline windows in each climate were already very good performers.

Orientation of the building may offer more advantages than window upgrades or shading, but credit for optimizing the orientation is not allowed in the 90.1 cost budget method. In order to assess the potential, we ran the baseline building simulations while varying the orientation. The results are shown in Table 8. Note that there are only four orientations since further rotation of the building would simply duplicate one of these four due to the nearly symmetrical design of the building.

Table 8 – Energy cost budget totals for the baseline building rotated to different orientations

Location	Baseline design costs	Baseline rotated 45° clockwise	Baseline rotated 90° clockwise	Baseline rotated 135° clockwise
Atlanta	\$32,946	\$33,538	\$33,376	\$33,378
Chicago	\$56,951	\$57,450	\$57,492	\$57,466
Houston	\$64,960	\$65,912	\$66,316	\$65,594

The difference between the worst orientation and the best orientation in Atlanta is 1.8%, just under 1% in Chicago, and slightly over 2% in Houston. Although orientation alone does not contribute anywhere near as much reduction as high efficiency HVAC equipment, it does provide greater improvement seen than most of the changes to the envelope which were simulated.

#### **Windows**

Although window orientation, shading, U-Factor, and SHGC can be varied in a proposed design to help comply with or exceed 90.1, the amount of window area is another factor influencing heat loss and gains through exterior walls. However, Table 11.3.1 in 90.1 is not completely clear as to whether a reduction in window area can be credited to the proposed design. In part 5 of the table, it suggests that all components of the envelope shall be identical except as identified in three specific exceptions. The exception dealing with fenestration requires the window area to be reduced to the maximum allowable by Section 5.5.4.2. It does not address what to do if the window area of the proposed design is less than the maximum (50% of wall area) for vertical fenestration).

In our simulations, the window area for the proposed and reference designs were the same. Energy Gauge only allows the areas to differ if the proposed design is greater than the 50% threshold. In this case, the reference building is set to 50% but the proposed design is set to the actual amount in the building.

One might ask why a building would be penalized for exceeding the 50% threshold but not given credit for being under the threshold. One possible answer is that the 90.1 energy cost budget method does not want to give credit for a building that was designed with an excessive amount of windows that was never intended to be built. However, it seems that picking a reasonable average or typical window area for a given building type should not be difficult and giving credit for reducing window areas below that area should result in a credit toward compliance under the energy cost budget method.

There is a practical limit to how much this can be reduced if it were included as an acceptable item in the energy cost budget method. Other code requirements for ventilation, natural light, and emergency egress would establish a lower limit of window area.

As an example of how much energy cost is at stake with window area under the 90.1 energy cost budget method, we reduced the window area from five windows per unit on north and south facing walls to two windows and from three to one window on the east and west sides. This is probably an extreme example for an apartment building, since it would cover emergency egress in a bedroom and leave only one to two other windows (depending if a center or end unit) for other rooms. None the less, for the Houston building the reduction in the total energy costs for the proposed design decreased by 1-1/2% under this scenario. Although this does not compare in magnitude to the

improvements available with high efficiency HVAC equipment, it does compare well to the other envelope improvements.

### COST ESTIMATES FOR EFFICIENCY UPGRADES

For each of the locations, the cost to achieve specific thresholds relative to ASHRAE 90.1 is summarized in Tables 9, 10 and 11. Costs do not include any utility company or tax incentives that may exist as these are limited by statute or program and/or vary by location.

Table 9 - Atlanta Costs

	Improvements re	quired to m	neet 15% o	30% thres	hold (actual	is 31%)	
System	System items	Units in building	Sq. Ft. in building	Cost per unit or Sq. Ft.	Baseline building costs	Cost with improvements	Cost difference
	SEER 12, 7.4 HSPF air source heat pump	32		\$4,038	\$129,200		\$62,800 to
Heat pump	3.7 COP, 16.9 EER ground source heat pump	32		\$6,000 - \$12,000		\$192,000- \$384,000	\$254,800
Total							
	Maximum imp	rovement	over 90.1 r	eference (3	9%)		
	SEER 12, 7.4 HSPF air source heat pump	32		\$4,038	\$129,200		\$62,800 to
Heat pump	3.7 COP, 16.9 EER ground source heat pump	32		\$6,000 - \$12,000		\$192,000- \$384,000	\$254,800
Attic	R-38		3168	\$0.47	\$1,489		\$412
7 ttto	R-49		3168	\$0.60		\$1,901	ΨΤΙΖ
Exterior walls	R-13 wood frame		8871	\$2.95	\$26,169		\$6,831
Exterior Wallo	R-21+5 wood frame		8871	\$3.72		\$33,000	ΨΟ,ΟΟΊ
Windows	Closest commercially available meeting both max U and max SHGC	200	2700	\$8.00	\$21,600		\$5,400
	Advanced window (U= 0.3, SHGC=0.19)	200	2700	\$10.00		\$27,000	
Exterior doors	R-2.6 steel	8		\$129.00	\$129		\$0
Exterior doors	R-5.2	8	-	\$129.00	\$129	\$0	φυ
Slab insulation	R-0		3168	\$0.00	\$0		
	R-5 XPS		3168	\$0.53		\$1,679	\$1,679
Total	Panlit avatam was prised					gar on the market	\$77,122 to \$269,122

Note: a 13 SEER split system was priced for this exercise. SEER 12 equipment is no longer on the market, even though this is the minimum efficiency permitted in 90.1-2004.

Table 10 - Chicago Costs

			- Unicag		notual is 169/	<u> </u>	
	Improvements i	required to	meet 15%	inresnoia (a	actual is 16%	o) 	
System	System items	Units in building	Sq. Ft. in building	Cost per unit or Sq. Ft.	Baseline building costs	Cost with improvements	Cost difference
	00 4545	00		ФО 000	#00.0F0		
Heating	80 AFUE gas furnace	32		\$2,083	\$66,656		\$73,216
	96 AFUE gas furnace	32		\$4,371		\$139,872	
Total							\$73,216
Impressomente regui	ized to most 200/ threeh		io 270/\				
improvements requi	ired to meet 30% thresh	loiu (actuai	15 31 70)				
Heating and cooling	80 AFUE gas furnace	32		\$2,083	\$66,656		
	12 SEER AC	32		\$4,038	\$101,600		\$23,744 to \$215,744
	3.7 COP, 16.9 EER ground source heat pump	32		\$6,000 - \$12,000		\$192,000- \$384,000	<b>4</b> =10,711
Total							\$23,744 to \$215,744
Maximum improvem	 nent over 90.1 reference	(46%)					
Exterior wall	R-13 wood frame	(1010)	3168	\$3.55	\$11,244		
Exterior wall	R-40 SIPs		3168	\$9.16		\$29,032	\$17,788
Attic	R-38		8871	\$0.60	\$5,360		
	R-49		8871	\$0.78		\$6,911	\$1,552
Subslab	R-0 R-5 XPS		8871 8871	\$0.00 \$0.68	\$0	\$6,071	\$6,071
Heating and cooling	80 AFUE gas furnace	32	0071	\$2,083	\$66,656	\$0,071	φο,στι
	12 SEER AC	32		\$4,038	\$101,600		\$23,744 to
	3.7 COP, 16.9 EER ground source heat pump	32		\$6,000 - \$12,000		\$192,000- \$384,000	\$215,744
Total	t avotom was priced for the						\$49,155 to \$241,155

Note: a 13 SEER split system was priced for this exercise. SEER 12 equipment is no longer on the market, even though this is the minimum efficiency permitted in 90.1-2004.

Table 11 - Houston Costs

		Table 1	<u> 1 – Houst</u>	on Costs			
	Impro	vements re	quired to m	eet 15% th	reshold	T	T
System	System items	units in building	Sq. Ft. in building	Cost per unit or Sq. Ft.	Baseline building costs	Cost with improvements	Cost difference
Heat pump	SEER 12, 7.4 HSPF air source heat pump SEER 15, 8.3 HSPF	32		\$4,038	\$129,200		\$77,200
Exterior wall	air source heat pump R-13 wood frame R-40 SIPs	32	3168 3168	\$6,450 \$2.86 \$6.79	\$9,055	\$206,400 \$21,523	\$12,469
Attic insulation	R-38 R-49		8871 8871	\$0.45 \$0.58	\$3,992	\$5,145	\$1,153
Windows	Best commercially available meeting both max U and max SHGC Advanced window (U= 0.3, SHGC=0.19	200	2700 2700	\$8.00 \$10.00	\$21,600	\$27,000	\$5,400
Total							\$96,222
Improvements	required to meet 30% thi	rochold (act	ual improv	omont is 41	0/ \		
Heat pump	SEER 12, 7.4 HSPF air source heat pump 3.7 COP, 16.9 EER ground source heat pump	32	•	\$4,038 \$6,000 - \$12,000	\$129,200	\$192,000- \$384,000	\$62,800 to \$254,800
Total				. ,		. ,	\$62,800 to \$254,800
Maximum impr	ovement over 90.1 refere	ence (48%)	Γ	Γ	Г	T	
Exterior wall	R-13 wood frame R-40 SIPs		3168 3168	\$2.86 \$6.79	\$9,055	\$21,523	\$12,469
Attic insulation	R-38		8871	\$0.45	\$3,992		\$1,153
	R-49		8871	\$0.58		\$5,145	, ,
Windows	Best commercially available meeting both max U and max SHGC	200	2700	\$8.00	\$21,600		\$5,400
	Advanced window (U= 0.3, SHGC=0.19	200	2700	\$10.00		\$27,000	
Hoot nums	SEER 12, 7.4 HSPF air source heat pump	32		\$4,038	\$129,200		\$62,800 to
Heat pump	3.7 COP, 16.9 EER ground source heat pump	32		\$6,000 - \$12,000		\$192,000- \$384,000	\$254,800
Total  Note: a 13 SEE	R split system was priced i	for this exerc	cise. SEER	12 eauipme	nt is no longe	er on the market ev	\$81,822 to \$273,822 en though

Note: a 13 SEER split system was priced for this exercise. SEER 12 equipment is no longer on the market even though this is the minimum efficiency permitted in 90.1-2004.

There is no single source for construction cost data. RS Means, Craftsman and others publish estimating guides, but they do not cover every system or subsystem nor every variation within a type of component. Thus, our cost estimates were derived from multiple sources including published data and quotes from suppliers and contractors in each city.

Exterior wall system costs were obtained from RS Means 2006 and 2007 *Residential Cost Data*, with location factors applied for the different cities. R-5 continuous insulation costs were also obtained from RS Means. All other insulation costs were obtained from supplier quotes in each city.

Window cost estimates were based on quotes from building supply outlets. As much as possible, costs were estimated within a manufacturer's brand and particular product line to ensure that the only difference in price was due to thermal improvements in glazing, versus changes in style or material quality. Incremental costs of windows were then normalized according to square footage, arriving at a single incremental cost per square foot for high performance windows. Because multiple quotes were returned from suppliers in Chicago and Houston versus none in Atlanta with the same window types, we elected to combine all quotes for each window type and use an average cost independent of location cost factors. We believe this is acceptable because the incremental cost of windows in all of the quotes was fairly consistent, and the incremental cost is our main interest.

Window jamb extensions were not included in costs. The cost of extensions could range from zero to \$30 or more per window. It is likely that the baseline building and the upgraded building would both be built using 2x6 or wider studs. Thus, there would be no jamb extensions due to increased cavity insulation. The exceptions would be when a 10 inch SIPs wall or continuous insulation is used. With one-inch continuous insulation is it sometime possible to order a wider frame at little to no added cost. Other options include purchasing jamb extensions or trimming them out onsite. With the 10 inch SIPs wall, custom made extensions would be required.

The costs of furnaces, heat pumps, air conditioners, and ground source heat pumps were estimated based on quotes from contractors. Ducted systems were chosen for the heating and cooling systems. Contractor-sourced quotes included material and labor. Air conditioners, furnaces, and air source heat pumps were priced as turnkey systems minus the material and labor costs of the duct system. We assumed that an identical duct system would be required for all systems, so this component was excluded from the quotes. Results indicated that the pricing was less dependent on geography than on the discretion of the individual contractor, so all quotes were averaged together to estimate the retail cost of installed systems at 1.5 tons. No volume-based discounts were sought when seeking quotes.

Cost for ground source heat pumps are highly variable and heavily dependent on drilling conditions, soil thermal conductivity and soil composition. For large, multifamily

projects, test wells are typically drilled on-site and soil thermal conductivity tests run to determine the loop field size required to match the heating and cooling loads of the units. Due to the large variability of loop field sizes and installation costs, turnkey costs for geothermal heat pumps were taken as a range that was normalized on a per ton basis. This range was based on contractor quotes and industry data. Quotes did not include the cost of the duct system. A vertical, closed loop system was assumed for the analysis. We recognize that the range of costs for a GSHP is wide, but this is reflective of the market that exists for this technology.

Since we were not able to reach the 50% threshold in any of the locations, we assumed that the remaining energy cost to do so would need to be made up by other means. We provided the costs for PV as one example in Table 12.

There may be options other than PV that can be used to make up the deficits in each location. In any case, applying them would require a change to the ASHRAE 90.1 scope. If for example, lighting were added to the scope for dwelling units, then something as simple as using CFLs might provide enough savings to reach the 50% threshold in Chicago and Houston. Other improvements such as high efficiency water heaters would likely be needed in Atlanta.

Table 12 - PV costs to meet 50% threshold

	Atlanta	Chicago	Houston
Normalized low-end cost of installed system (\$/W DC)	\$7.00	\$7.00	\$6.00
Normalized high-end cost of installed system (\$/W DC)	\$9.00	\$9.00	\$8.0 0
Total low-end cost of PV system (\$)	\$240,885	\$154,778	\$42,527
Total high-end cost of PV system (\$)	\$309,709	\$199,000	\$ 56,703

PV costs were based on turnkey installation quotes from suppliers. No battery storage was included. The systems were based on a net metering set-up where the electricity generated from the PV panels was sent back to the grid. Because of a wide variety in quotes, PV costs are expressed as a range from the low to high end. As mentioned previously, tax credits that may be available are not considered in the costs.

### **DISCUSSION/CONCLUSIONS**

The use of energy simulations with various models is a recognized method for determining compliance in most major building codes and standards. Chapter 11 of the ASHRAE Standard 90.1 provides for the use of a cost budget method to assess how much better or worse a building would perform relative to the requirements of the standard.

While simulations using the energy cost budget method offer opportunity for more flexibility than following the prescriptive requirements, it is worth noting that this option

may be not be all that practical for a building owner or designer. The effort to run multiple simulations for a building is no small task for a complex building. Costs associated with modeling will be a significant barrier on many projects. Thus, it is not uncommon for even leading edge designers/builders to strive to meet the prescriptive requirements of ASHRAE 90.1 rather than run simulations.

The simulation results and other estimates from this work suggest that reaching a goal of 15% better than ASHRAE 90.1-2004 may not be that difficult from a technical and practical view point. However, the traditional approach of improving the insulation levels in the building envelope will not achieve this level of performance, and will not even begin to approach the 30% and 50% improvement levels. The impact of envelope improvements over current practice is small even in combination with other similar envelope improvements.

In order to make substantial gains against the backdrop of the 2004 90.1 standard, higher efficiency equipment will be a core component of most designs of apartment buildings in the range of four stories or less. At the 15% level, this was accomplished in two of the three cities we examined with what might be termed conventional high efficiency equipment, including air source heat pumps and AC units or natural gas furnaces. The technology for these systems exists and is commercially available through typical supply channels.

Reaching the 30% level is possible in all three climates for the buildings we simulated, but efficiency of the HVAC equipment needed to do so would require advanced technology. For an apartment building with separate heating and cooling systems, a ground source heat pump (GSHP) is the technology most likely to provide this efficiency. In fact, GSHP technology would likely reach the 30% target in all three locations we examined even without other improvements to the buildings. It is commercially available, but is still very much a specialty product. The vast majority of buildings do not use this technology and the level of experience with it by trade contractors is limited. Despite a growing market share, the infrastructure for GSHPs is still in an early state of development in many areas.

We were not able to reach the 50% level in Atlanta, Houston, or Chicago with the apartment building we studied. Every building is different, so it may be possible to reach the 50% level using high efficiency GSHP technology and significantly enhancing the envelope for other building designs. In any case, the 50% threshold is a very optimistic goal and may not be feasible without significant changes to the scope of 90.1 or significant improvements in technologies.

Although the 15% and 30% goals can be achieved in these cities, the cost to do so is significant. Table 13 shows the cost of combinations of technologies that most closely match the various levels of performance. The table also shows costs for the maximum levels obtained.

Table 13 – Costs and simple payback for various levels of performance over 90.1 for three cities

various levels of performance over 30.1	ioi tinice e	11103
Atlanta	% better than 90.1	Added cost in dollars
GSHP (3.7 COP, 16.9 EER)	31	\$62,800 to \$254,800
R-49 attic, R-21+5 walls, advanced windows (U=0.3, SHGC+0.19), R-5.2 door, R-5 subslab insulation, GSHP (COP 3.7, EER 16.9)	39	\$77,122 to \$269,122
Chicago		
96 AFUE furnace	15	\$73,216
GSHP (3.7 COP, 16.9 EER)	37	\$23,744 to \$215,744
R-49 attic, R-40 walls, R-5 subslab insulation, GSHP (3.7 COP, 16.9 EER)	46	\$49,155 to \$241,155
Houston		
SEER 15 HP w/ 8.3 HSPF, R-40 walls, R-49 attic, advanced windows(U=0.3, SHGC+0.19)	15	\$96,222
GSHP (3.1 COP, 14.6 EER)	41	\$62,800 to \$254,800
R-40 walls, R-49 attic, advanced windows, GSHP (3.1 COP, 14.6 EER)	48	\$81,822 to \$273,822

The costs do not include additional design costs that will be incurred. With prescriptive changes to the 90.1 standard (meaning that prescriptive pathways were established to meet higher efficiency levels), the added design costs would be minimized. If simulations are required (e.g., a performance approach), then the design costs could be significant. Results from projects like this can be useful in reducing analysis costs by showing designers the most likely pathways for reaching a specific level of improvement.

One key finding relative to costs is that GSHPs have a wide range of costs associated with them. Even on the low end, they are quite expensive compared to conventional heat pumps and air conditioners. One interesting finding is that a large portion of the cost of a GSHP in a location like Chicago could be offset if a gas furnace with separate AC unit is used as the baseline. This same type of offset would also be available with a high efficiency conventional heat pump, since in either case, the proposed design would replace two systems (AC and gas furnace) with one system (a heat pump).

In terms of realizing the energy cost savings tied to high performance multi-family buildings, the renter in an apartment would see the savings benefits while the builder/owner would incur the costs. There is no evidence to suggest that the increased costs could be returned to the owner in the form of higher rents. It is easy to see where excessive upfront costs, if they eat into profits or inhibit financing, may be the deciding factor in whether to construct a multi-family building in the first place. This could have the unintended consequence of limiting housing choices in the market and driving renters, many of whom struggle with housing costs, into older, less efficient buildings with higher monthly utility costs.

Simple payback expressed in years is one way to analyze the costs and benefits of an improvement. This approach would only be applicable where the building owner is also the party responsible for paying the utilities. Very few new apartments would fall into this category, so for the payback analysis to have any credibility, we need to assume that there is some other way that the benefits are accruing to the owner.

A simple payback is typically expressed as the number of years it would take for estimated energy savings to offset the initial additional costs of construction. We elected to examine only the paybacks for Atlanta, since the Atlanta baseline building was almost identical to a minimum 90.1 building. (See Appendix C for a discussion on the baseline versus reference designs). Atlanta provides the cleanest comparison of performance versus costs of the three cities.

The paybacks for Atlanta are shown in Table 14. Note that there is no consensus on what is an acceptable timeframe for a simple payback. In the United States, valid arguments have been made for as little as 3 years or as high as 7 to 10 years in regard to energy efficiency in buildings. The paybacks in Table 14 exceed even the higher range of what is acceptable on average in the United States, and substantially exceed them at the high end of the cost estimates for given building system packages.

Internationally, there are different perspectives than in the United States. Recent proposals in the EU are attempting to designate 30 years as the basis for payback analysis.

Table 14 – Cost and payback for selected improvements in Atlanta

Building system package	% better than 90.1	Simple payback in years <sup>1</sup>
	31 (closest set of	16 (25)
	improvements achieving at	
GSHP (3.7 COP, 16.9 EER)	least 30%)	
R-49 attic, R-21+5 walls, advanced windows (U=0.3,		14 (21)
SHGC+0.19), R-5.2 door, R-5 subslab insulation, GSHP	39 (maximum achieved in	
(COP 3.7, EER 16.9)	simulations)	

<sup>&</sup>lt;sup>1</sup>Costs and thus payback of GSHPs vary greatly. The paybacks are based on an average of the high and low end of estimated costs. The payback associated with the high end of the cost estimates is shown in ().

Other findings from this study that could be helpful to builders, building owners, and designers include:

Running a simulation on a building that is marginally out of compliance with
prescriptive requirements in a code or standard may be all that is required to
comply. When we developed a baseline building in the modeling software using
prescriptive minimums from 90.1, the buildings in Houston and Chicago passed
with plenty of room to spare.

- One of the reasons for surpassing the reference design by such a wide margin is related to the way that the reference building's HVAC system is determined. For example, in Chicago, the reference building was assigned a boiler even though a natural gas furnace was used in the proposed design. The 90.1 committee should develop criteria so that the same system is used in proposed and reference buildings.
- There is a disconnect between what is available on the market and the minimum requirements in energy codes and standards. For example, in order to meet window requirements, a designer has to select a window that meets the SHGC and the U-Factor requirements. Unfortunately, there are not any windows found that meet both of these criteria in the NFRC listings for major window manufacturers. Because we selected products that were at or below (better than) the SHGC, we ended up with a U-Factor much lower than the maximum. Thus, common products or practices in today's buildings by themselves can result in much better performance than minimum code or standards requirements.
- HVAC equipment is often not available at higher efficiencies in the same size or capacities as less efficient equipment. Finding a SEER 19 heat pump for a 12,000 Btu through-the-wall heat pump would be a challenge.
- Fan energy assumptions for relatively small equipment found in apartments and similar spaces are not well documented. Yet fan energy can be a significant consumer of energy for heating and cooling. Many simulation tools including Energy Gauge default to 0.9 watts/cfm based on requirements for larger equipment taken from 90.1. Recent work in California and Florida suggest that actual power for heat pumps depends on the size of the units (Wilcox et. al., Workshop Presentations, 2008 California building energy efficiency standards, July 12, 2006 and Parker and Proctor, Hidden power drains: Trends in residential heating and cooling fan watt power demand, Florida Solar Energy Center, 2001). For sizes typically used in homes and apartments, the range is from about 0.4 to 0.55 watts/cfm. In our simulations, we did not look at changing the fan energy consumption as a way to improve the performance of the proposed design. As more information develops through research and data from manufacturers, fan energy could be an area where significant energy savings could be realized and applied to code compliance.
- As building envelopes improve, HVAC systems can be downsized to reflect smaller loads. These changes were not considered in this study because there are practical limitations to how small a unit can be in a building. For example, it is difficult to find a 30,000 Btu gas furnace, even though this capacity may be adequate for a given building space.
- Standards and codes, including 90.1, are not perfect nor do they always match
  up well with simulation tools. When running simulations, a designer must make
  some assumptions when guidance is not provided in the standard. User bias
  and other factors can often make a difference in whether a building complies with
  a specific standard or code.

 ASHRAE must consider changes to what is within the scope of covered items in 90.1 and the energy cost budget method in Chapter 11of the standard if the 50% goal is to be achieved. Water heating energy use, lighting inside dwellings, building orientation, and infiltration are examples where benefits could be obtained if brought into the energy cost budget method.

Although it may be outside the scope of this study, one comment relative to the declared goals of the ASHRAE president and the Department of Energy is worth noting. The consensus process has served both regulators and industry well in bringing many different points of view into the development of standards for the building industry. It is a well respected process worldwide. Further, ASHRAE 90.1 has a long history of basing committee decisions on strong technical support. Declaring that 90.1 will be a certain percentage better than today in future editions may unduly influence the consensus process. Although the idea of improving building performance is good, the process needs to be respected so that all points of view, economic benefits, practical limitations, and other issues are understood and considered.

Finally, policy makers and standards developers should recognize that the market infrastructure, climate, and consumer preferences all influence the design of a building. Climates and markets can be radically different around the United States. Approaches that seem reasonable in one part of the country should not automatically be adopted elsewhere. In some climates where more energy is used, it may be reasonable and more cost-effective to expect more efficiency improvements compared to buildings in milder climates.

### APPENDIX A - SELECTION OF ENERGY GAUGE PREMIER SUMMIT

Using energy simulation models to assess the impacts of going beyond 90.1-2004 could be fairly involved because some models do not yet create a default code-compliant building. This means that programs like Visual DOE, Energy 10, TRYNSYS, Energy Plus, EQUEST and others – while extremely powerful tools – do not automatically create a 90.1-compliant version of a building design for the sake of comparison. Instead a user must essentially construct two models, one for the actual design and one that meets the minimum requirements of 90.1 (usually called the budget building or the reference building).

Modeling a reference building, like any building simulation, requires some assumptions on the part of the user. It also is susceptible to "gaming" the system (i.e., reaching compliance by making favorable but not necessarily realistic assumptions), although 90.1 does try to limit this with very specific instructions on how to develop the reference and design buildings. None-the-less, by carefully selecting inputs that would be within the range of typical or acceptable, one user could get a marginal building to pass while another user's assumptions might show the same building as failing to meet the standard. To take any subjective decisions out of the process of creating a reference design, we focused on tools that automatically develop the reference.

Although there may be some lesser-known simulation tools out there somewhere that automatically create a reference building in accordance with the 90.1 energy cost budget method, we were able to identify only two commercially available tools - Energy Gauge Premier Summit, available from the Florida Solar Energy Center, and REM Design, available from Architectural Energy Corporation. Of these two, only Energy Gauge meets the requirements for simulation tools specified in 90.1. REM Design, although a useful tool for other purposes, is not an hourly simulation tool as required by Chapter 11 of 90.1. It can only be used with special approval, for example if it could assess options that other tools do not address. Thus, Energy Gauge was the tool used for most of the simulations in this study.

Energy Gauge Premier Summit (EG) is a front end developed to run the DOE2 simulation tool. It allows the user to develop a model of their building and then interfaces with the DOE2 software for the simulations. EG can produce a DOE 2 base simulation report, Florida Code compliance reports, and various ASHRAE 90.1 compliance reports including the energy cost budget method. It also runs a check against ASHRAE 140 to show that EG meets the requirements ASHRAE specifies for a simulation tool.

Our selection of EG for this study does not imply that it is somehow superior to the other available simulation tools. What it does show is that care should be taken in selecting a simulation tool. A simulation tool that is good for our purpose may not be the best tool for a designer or for assessing items like temperature fluctuations across thermal zones. All of the tools have advantages and disadvantages depending on specific objectives of the user.

A word of advice is also offered when trying to compare results from different simulation tools. The results from EG simulations we ran do not represent energy use in the

building. Rather, they indicate the energy use and costs associated with what is regulated within the scope of 90.1. These are two very different items.

Results from models will also vary, sometimes greatly, from actual energy use in a building. Reasons for this include differences in actual weather versus historical data used in the models, assumptions that must be made by the user when inputting a specific building (for example, an unusual geometry may need to be approximated), or occupants effects. Perhaps the best use of modeling is to compare the relative performance of a building assuming different practices and materials. Thus, these tools fit well within our objectives.

As with any simulation tool, EG has some limitations. Among the most significant of these are limits on the types of HVAC systems that can be modeled. For example, geothermal heat pumps can not be modeled in EG. Likewise, economizers can not be modeled with the current version of EG. Another limitation is that the floor module does not allow one to model perimeter slab insulation, only under-slab insulation. Most of these are not significant issues when modeling a multi-family building. In the case of geothermal heat pumps, however, we did need to change to a different simulation tool to assess the improvement that these systems could achieve.

EG also does not allow the user to modify the natural air exchange rate (infiltration) in a building. This is not an issue from the perspective of compliance with ASHRAE 90.1 since 90.1 does not regulate infiltration from a performance perspective but rather requires sealing of specific openings in the envelope in prescriptive fashion. Reducing infiltration in a building will result in significant energy savings and ASHRAE and Energy Gauge should both consider allowing this parameter to be modified with credit given for lower infiltration rates.

Infiltration is not the only area where EG and ASHRAE do not allow modifications to a building to be credited relative to compliance in a multi-family building. Water heating, building orientation, and lighting within dwellings are two other areas where great improvements can be made to a building if 90.1 (and compliance simulation tools) was structured to recognize these improvements.

Additionally, EG does not allow a ventilated attic. Thus, it may introduce some minor difference compared to the un-vented (but unconditioned) attic we used in our simulations. Similar issues are present in nearly all simulation tools – they all have limitations. This makes it difficult to compare results from one model to another, or to use models to predict energy use. However, EG and other simulation models are good tools for comparing the relative performance of buildings and to check against compliance with 90.1 and other codes and standards.

Last, EG does not offer some typical options for foundation insulation. As mentioned above, when we simulated subslab insulation, the entire under slab area was assumed to be insulated as opposed to the practice of just insulating two to four feet at the perimeter.

Like other simulation tools, EG is continually being improved. We have coordinated closely with the developers at Florida Solar Energy Center (FSEC) on this project and they have been grateful for feedback that is already being incorporated into future revisions of the software. The FSEC staff offered help throughout the project and even ran our base building in their debug mode to confirm that is was running correctly. However, Version 3.11 of EG that we are using has some issues that required modifications to the interpretation of the results. The issues we encountered were two fold.

First, the cost budget report in EG takes the reference building and proposed building designs and calculates "modified points" that are basically the percentage of compliance. In other words, the total energy costs for the proposed design are divided by the total costs for the 90.1 reference design. Thus a proposed design with a cost of \$20,000 would show a point value of 80.0 compared to a reference design with a cost budget of \$25,000. After consulting with FSEC, we concluded that the method of calculation has slight errors in the programming. Thus, we manually calculated the percentages rather than use the EG results.

Second, the floor module used by EG is being revised to more efficiently interface with the DOE2 simulation engine. Currently, the interaction between the two results in a slight to moderate change to the reference building's energy use and costs when subslab insulation is added to a building. A similar but very small change to the reference building occurs when the attic insulation is modified. These issues do not impact the calculation of the proposed design building's energy use or costs.

After conferring with FSEC, we determined that the EG calculations of the modified points were not accurate. For all such comparisons, we reverted to independent calculations comparing the proposed design to the base building reference design (remember that the reference design is the minimum requirement to comply with 90.1).

## APPENDIX B- BASE BUILDING INPUT FILES

# EnergyGauge Summit v3.11 INPUT DATA REPORT

## **Project Information**

Project Name: Baseline MFH Atlanta Orientation: North

Project Title: MFH code minimum building in Atlanta Building Type: Multi-Family

Address: Enter Address here Building Classification: New Finished building

Enter Address here

State: GA No.of Storeys: 4

Zip: 0 GrossArea: 44517 SF

Owner: NMHC

	Zones										
No	Acronym	Description	Туре	Area [sf]	Multiplier	Total Area [sf]					
1	Elevator zones	Elevator areas with mechanical space	UNCONDITIONED	96.0	1	96.0					
2	Attic	Attic	UNCONDITIONED	8973.5	1	8973.5					
3	DU SW 4	Dwelling unit SW corner on 4th story	CONDITIONED	1000.0	1	1000.0					
4	DU SE 4	Dwelling unit SE corner on 4th story	CONDITIONED	1000.0	1	1000.0					

5	DU NE 4	Dwelling unit on 4th floor at NE corner	CONDITIONED	1000.0	1	1000.0	
6	DU NW 4	Dwelling unit on 4th floor at NW corner	CONDITIONED	1000.0	1	1000.0	
7	DUN center 4	North DUs on 4th floor in center	CONDITIONED	2093.8	1	2093.8	
8	DUS center 4	South DUs on 4th floor in center	CONDITIONED	2000.0	1	2000.0	
9	DU SW 1	Dwelling unit SW corner on 1st story	CONDITIONED	1000.0	1	1000.0	
10	DU SE 1	Dwelling unit SE corner on 1st story	CONDITIONED	1000.0	1	1000.0	
11	DU NE 1	Dwelling unit on 1st floor at NE corner	CONDITIONED	1000.0	1	1000.0	
12	DU NW 1	Dwelling unit on 1st floor at NW corner	CONDITIONED	1000.0	1	1000.0	
13	DUN center 1	North DUs on 1st floor in center	CONDITIONED	2093.8	1	2093.8	
14	DUS center 1	South DUs on 1st floor in center	CONDITIONED	2000.0	1	2000.0	
15	DU N 2,3 center	Interior North DUs on 2nd and 3rd floors	CONDITIONED	4187.5	1	4187.5	
16	DU S 2,3 center	Interior south DUs on 2nd and 3rd floors	CONDITIONED	4000.0	1	4000.0	
17	DU SW 2,3	Dwelling unit SW corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
18	DU SE 2,3	Dwelling unit SE corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
19	DU NW 2,3	Dwelling unit NW corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
20	DU NE 2,3	Dwelling unit NE corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
21	Cor 4	4th floor corridor	CONDITIONED	768.0	1	768.0	
22	Cor 1	1st floor corridor	CONDITIONED	768.0	1	768.0	
23	Cor 2,3	2nd, 3rd floor corridors	CONDITIONED	1536.0	1	1536.0	

Spaces											
No	Acronym	Description	Туре	Depth [ft]	Width [ft]	Height [ft]	Multi plier	Total Area [sf]	Total Volume [cf]		
	elevator space	zones e combined elevator and motor/controls room	Electrical Mechanical Equipment Room - General	8.00	12.00	35.00	1	96.0	3360.0		
In Zone	: Attic attic space	attic space with average height assumed	Storage & Warehouse - Inactive Storage	68.50	131.00	8.50	1	8973.5	76274.8		
	DU SE Roof	individual dwelling unit	Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		
In Zone	DU SE 4		Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		
In Zone	: DU NE 4 DU NE 4		Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		
In Zone	DU NW 4	DU on NW corner of 4th story	Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008		
In Zone			Private Living Space	31.25	33.50	8.00	2	2093.8	16750.0		
In Zone			Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0		
In Zone	DU SW 1		Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		
In Zone 1	: DU SE 1 DU SE 1	The same and the s	Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008		
In Zone	: DU NE 1 DU NE 1		Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		
In Zone	: DU NW DU NW 1		Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		

No	Name			Simple Construct	Massless Construct	Conducta [Btu/h.sf.		Density [lb/cf]	RValue [h.sf.F/Btu]	
1070	ASHRAE Apper	ndix roof R-3	38	No	Yes	0.03			37.0	
	Layer	Material No.	Material		Th	ickness [ft]	Framing Factor			50° (5)
	1	1012	R-38 roof truss A	SHRAE App.						
No	Name			Simple Construct	Massless Construct	Conducta [Btu/h.sf.		Density [lb/cf]	RValue [h.sf.F/Btu]	
1071	R-19 generic flo	or insulation		No	Yes	0.05			19.0	
	Layer	Material No.	Material		Th	ickness [ft]	Framing Factor			
	1	1014	R-19 Generic Inst	ulation	0.	4147	0.000			

In Zone: Attic	c							
In Space:	attic space 1 Incandescent	General Lighting	18	60	1080	Manual On/Off	4	
	SW 4							
	DU SE Roof  1 Compact Fluorese	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU S In Space:	DU SE 4							
	<ol> <li>Compact Fluorese</li> </ol>	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU ! In Space:	NE 4 DU NE 4							
	1 Compact Fluorese	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU I	NW 4 DU NW 4							
	1 Compact Fluorese	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	N center 4 DU N center 4							
2000 M - 100 M	1 Compact Fluoresc	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	S center 4							
	DU S center 4 1 Compact Fluoresc	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU S In Space:	SW 1 DU SW 1							
	1 Compact Fluorese	cent General Lighting	18	18	324	Manual On/Off	1	
	2 Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU S	SE 1							36=33
In Space:	DU SE 1 1 Compact Fluoresc	cent General Lighting	18	18	324	Manual On/Off	1	

In Zone										24-03
1	DU N center	DU north in center of	Private Living Space	31.25	33.50	8.00	2	2093.8	16750.0	
In Zone	: DU S cer	lst story								
		DU south in center of	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	П
		1st story	Titale Bring space		02.00					_
In Zone										<u> </u>
1	DU interior N	oDUs in interior of 2nd	Private Living Space	31.25	33.50	8.00	4	4187.5	33500.0	
	DUGGG	and 3rd follrs								
In Zone			Private Living Space	31.25	32.00	8.00	4	4000.0	32000.0	П
	Do center so	3rd floors	Tivate Living Space	31.23	32.00	0.00	7	4000.0	32000.0	ш
In Zone	: DU SW									
1	DU SW 2,3	individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	: DU SE 2	.3								
	DU SE 2,3	individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	: DU NW	23								_
		individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone		Č	0 1							_
	DU NE 2,3	بى individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
		man idair aweining and	Tivate Biving Space	51.25	52.00	0.00	L	2000.0	10000.0	ш
In Zone	c: Cor 4 Corridor 4	Corridor space on 4th	Carridae	128.00	6.00	8.00	1	768.0	6144.0	
1	Corridor 4	floor	Corridor	128.00	0.00	8.00	1	708.U	0144.0	ш
In Zone	e: Cor 1	HOVI								
1		e.Corridor space	Corridor	128.00	6.00	8.00	1	768.0	6144.0	
In Zone	e: Cor 2,3	676								
	Corr 2,3	Corridor space 2,3	Corridor	128.00	6.00	8.00	2	1536.0	12288.0	
		floors		.m. 75.50.50.50.1	2100		~			_

			Lighting	9				
No	Type	Category	No. of Luminaires	Watts per Luminaire	Power [W]	Control Type	No.of Ctrl pts	
	zones ator space Recessed Fluorescent - No vent	General Lighting	1	144	144	Manual On/Off	1	

	72	53: 5:			120				
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	NE 1	oleven)							
In Space:	DU N	E 1 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	Maria Company	6	7.5				
	-3.0		General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NW 1								
m space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N cen	ter 1							
In Space:		center 1 Compact Fluorescent	Consed Lighting	18	18	324	Manual On/Off		
	1		General Lighting					1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	S cent	ter 1 center bottom							
in space:	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N 2,3	center							
In Space:	DU in	nterior North							
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
		center							
In Space:	DU co	enter south Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	-77.0		General Lighting	0	00	300	Manual Off Off	1	
In Zone: DU In Space:	SW 2								
m space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	SE 2,3	3							
In Space:	DU S	E 2,3		1947		1227	100 100 000		
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	

	NW 2			·			·		
In Space:	DU N	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NE 2, DU N								
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: Cor									
In Space:	Corri	idor 4							
1.00	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	
In Zone: Con	. 1								
In Space:	Corri	idor spaces							
147500 <b>.</b>	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	
In Zone: Con	2,3								
In Space:	Corr	2,3							
•	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	

					Walls						
No	Description	Туре	Width I [ft]	H (Effec) [ft]	Multi plier	Area [sf]		Conductance [Btu/hr. sf. F]	Heat Capacity [Btu/sf.F]	Dens. R-Value [lb/cf] [h.sf.F/Btu	
In Z	Cone: Elevator zone	s									15
1	East facing elevator wall 1st floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	East	0.0890		11.2	
2	East facing elevator wall 2,3 floor	R-13 wall 16 OC Ashrae App	12.00	8.00	2	96.0	East	0.0890		11.2	
3	East facing elevator wall 4th floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	East	0.0890		11.2	
4	West facing elevator wall 1st floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	West	0.0890		11.2	
5	West facing elevator wall 2,3 floor	R-13 wall 16 OC Ashrae App	12.00	8.00	2	96.0	West	0.0890		11.2	

6	West facing elevator wall			0.00	4	000	***			
		R-13 wall 16 OC	12.00	8.00	1	96.0	West	0.0890	11.2	
7	4th floor	Ashrae App	0.00	0.00	1	64.0	37. 41.	0.0000	11.0	
7	North facing elevator	R-13 wall 16 OC	8.00	8.00	1	64.0	North	0.0890	11.2	ш
	wall 1st floor	Ashrae App							22.2	
8	North facing elevator	R-13 wall 16 OC	8.00	8.00	2	64.0	North	0.0890	11.2	
	wall 2,3 floors	Ashrae App								
9	North facing elevator	R-13 wall 16 OC	8.00	8.00	1	64.0	North	0.0890	11.2	
20. 10	wall 4th floor	Ashrae App								
(E) (E)	Zone: Attic									_
1	Attic gable end wall	Attic gable end wall	68.50	8.56	1	586.4	East	1.5827	0.6	
	facing east									_
2	Attic gable end wall	Attic gable end wall	68.50	8.56	1	586.4	West	1.5827	0.6	
	facing west									
In?	Zone: DU SW 4									
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App								
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
	walls	Ashrae App								200
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
In	Zone: DU SE 4									
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App								10000
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								-
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
		Ashrae App								
In										
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								12-33
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	corridor	Ashrae App								
In	Zone: DU NW 4									
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	walls	Ashrae App								
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
	walls	Ashrae App								
	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
3	vian between and and									
1 2 3 In 2 1	North facing exterior walls East facing exterior walls Wall between unit and corridor Zone: DU NW 4 North facing exterior walls West facing exterior walls	R-13 wall 16 OC Ashrae App R-13 wall 16 OC Ashrae App R-13 wall 16 OC Ashrae App R-13 wall 16 OC Ashrae App R-13 wall 16 OC Ashrae App	32.00 31.25 32.00 32.00 31.25	8.00 8.00 8.00 8.00	1 1 1	250.0 256.0 256.0 250.0	East South North West	0.0890 0.0890 0.0890 0.0890	11.2 11.2 11.2 11.2	

In Z	one: DU N center 4									722-111
1	North facing exterior	R-13 wall 16 OC	33.50	8.00	2	268.0	North	0.0890	11.2	
	walls	Ashrae App								
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
1200	between units	Ashrae App	22722	222	1020		220			_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
	between units Wall between unit and	Ashrae App	22.50	8.00	0	268.0	C 41	0.0890	11.0	
4	corridor	R-13 wall 16 OC	33.50	8.00	2	268.0	South	0.0890	11.2	ш
In 7	one: DU S center 4	Ashrae App								
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11.2	
	walls	Ashrae App	32.00	0.00	2	250.0	Douth	0.0070	11.2	_
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
	<b>3</b>	Ashrae App							,0.00.00	_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								
4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
1000000	one: DU SW 1	D 14 111100		0.00		25.0		0.0000		
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
2	walls West facing exterior	Ashrae App R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
2	walls	Ashrae App	31.23	0.00	1	230.0	West	0.0690	11.2	ш
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	corridor	Ashrae App	52.00	0.00		220.0	1101111	0.0070		_
In Z	one: DU SE 1									
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								_
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
17	corridor one: DU NE 1	Ashrae App								
1 1 1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
1	walls	Ashrae App	32.00	0.00	1	230.0	INOLUI	0.0690	11.2	ш
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
2	Trans facing executor walls	Ashrae App	31.20	0.00	1	200.0	Last	0.0070	11.2	_
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
200	corridor	Ashrae App		10 To TO TO TO	-5776	(T)547016				
In Z	one: DU NW 1	1.50								

1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256,0	North	0.0890	11	2	П
1	walls	Ashrae App	32.00	0.00	1	250.0	ivoitii	0.0070	111		_
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
170	walls	Ashrae App					0.0000		77		
3	Wall between unit and	R-13 wall 16 OC	8.00	32.00	1	256.0	South	0.0890	11	.2	
	corridor	Ashrae App									_
In 2	Zone: DU N center	1									
1	North facing exterior	R-13 wall 16 OC	33.50	8.00	2	268.0	North	0.0890	11	.2	
	walls	Ashrae App									
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
	between units	Ashrae App									
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11	.2	
	between units	Ashrae App									
4	Wall between unit and	R-13 wall 16 OC	27.50	8.00	2	220.0	South	0.0890	11	.2	
	corridor	Ashrae App									1.10
In Z	Zone: DU S center 1										
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11	.2	
	walls	Ashrae App									_
2	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11	.2	
- 62	between units	Ashrae App	0.000								_
3	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
	between units	Ashrae App	212/2/27	12022	1020	2200		12/12/2020	9.9	1020	_
4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11	.2	
I	corridor	Ashrae App									
100	Cone: DU N 2,3 cen		22.50	0.00		250.0	37. 1	0.0000	99		
1	North walls on interior	R-13 wall 16 OC	33.50	8.00	4	268.0	North	0.0890	11	.2	
	DUs	Ashrae App	21.25	0.00	•	250.0		0.0000		•	
2	East facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11	.2	
,	between units	Ashrae App	21.05	8.00	2	250.0	West	0.0000		^	
3	West facing walls between units	R-13 wall 16 OC Ashrae App	31.25	8.00	2	230.0	West	0.0890		.2	ш
4	Wall between unit and	R-13 wall 16 OC	27.50	8.00	4	220.0	South	0.0890	11	.2	
4	corridor	Ashrae App	27.50	8.00	4	220.0	South	0.0690	11	.2	ш
In 7	Cone: DU S 2,3 cent										
1	South walls on interior	R-13 wall 16 OC	33.50	8.00	4	268.0	South	0.0890	11	.2	
	DUs	Ashrae App	33.30	0.00	7	200.0	bouut	0.0050	11	. L	_
2	West facing walls	R-13 wall 16 OC	31.25	8.00	2	250,0	West	0.0890	11	2	
2	rrest facilig walls	Ashrae App	31.23	0.00	2	250.0	West	0.0050	11	.2	_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11	.2	
	Trust taonie wans	Ashrae App	31.23	0.00	2	250.0	Last	0.0020	11	. 2	_
		. made rapp									

4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	4	256.0	North	0.0890	11.3	2 🔲
In 7	corridor Cone: DU SW 2,3	Ashrae App								
11112	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11.3	2 🗆
	walls	Ashrae App	52.00	0.00	2	250.0	Doddi	0.0070	11	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	2	250.0	West	0.0890	11.3	2 🗆
150	•	Ashrae App								_
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.2	2 🗆
	corridor	Ashrae App								
In Z	Zone: DU SE 2,3									
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11.3	2 🗆
_	walls	Ashrae App	21.25	0.00		250.0	***	0.0000	990	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11.3	2 🗆
3	Wall between unit and	Ashrae App R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.3	2 🗆
3	corridor	Ashrae App	32.00	0.00	2	250.0	Notur	0.0690	11	. Ц
In 7	Zone: DU NW 2,3	risinae ripp								
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.3	2 🗆
	walls	Ashrae App								_
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	2	250.0	West	0.0890	11.3	2 🗆
657.6	walls	Ashrae App								-
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11.3	2 🔲
	corridor	Ashrae App								
22000	Zone: DU NE 2,3	D 10 111600	** **	0.00		2550				
1	South facing exterior walls	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.3	2 🗆
2	East facing exterior walls	Ashrae App R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11.3	2 🗆
	East facing exterior wans	Ashrae App	31.23	0.00	2	230.0	East	0.0690	11	. <u>П</u>
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11.3	2 🗆
. T.	corridor	Ashrae App	52.00	0.00	-	200.0	bouni	0.0070	****	_
In Z	Cone: Cor 4	11								
1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	1	48.0	East	0.0890	11.3	2 🗆
A8010	east	Ashrae App								
2	Corridor wall facing west	R-13 wall 16 OC	6.00	8.00	1	48.0	West	0.0890	11.2	2 🗆
		Ashrae App								
152	Cone: Cor 1		10000		142				1000	_
1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	1	48.0	East	0.0890	11.3	2 🗆
2	east	Ashrae App R-13 wall 16 OC	6.00	8.00	1	48.0	West	0.0890	11.3	2 🗆
2	Corridor wall facing west	Ashrae App	0.00	8.00	1	48.0	west	0.0890	11.3	
In 7	Cone: Cor 2,3	venue whh								
IIIZ	one. Cut 2,0									

1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	2	48.0	East	0.0890	11.2	
2	east Corridor wall facing west	Ashrae App R-13 wall 16 OC Ashrae App	6.00	8.00	2	48.0	West	0.0890	11.2	

					Windo	ws						
	No	Description	Туре	Shaded	U [Btu/hr sf F]	SHGC	Vis.Tra	W [ft]	H (Effec) [ft]	Multi plier	Total Area [sf]	
In Zone: DU In Wall:												
in wan:	2	North windows	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
In Zone: DU	J N ce	nter 1										_
In Wall:	N ext											
	1	North windows	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
In Zone: DU	7.00											
In Wall:	N ext	wall North windows	User Defined	No	0,5000	0.38	0.35	3.00	4.67	5	70.1	
In Zone: DU			User Defined	NO	0.5000	0.38	0.55	3.00	4.07	3	70.1	
In Zone: Du												
III (vaiii	1	East windows.	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Wall:	N ext	wall										-
	1	North windows,	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
In Zone: DU	J NE	2,3										
In Wall:												_
		East windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Wall:			** ** ** *			0.00		2.00		_		_
	1	North windows	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
In Zone: DU In Wall:												
III wall:	E EXU	East windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Wall:			Con Domina	1.0	0.1000	0.20	0.15	5.50		-		
		North windows,	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
		approx. 70 SF										_
In Zone: DU												
In Wall:			II - D C - I	37	0.5000	0.20	0.25	2.00	1.67	-	70.1	
Y., XX7. 11	1	North windows	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
In Wall:	W Ex	t walls West windows,	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
	1	west windows,	Oser Defined	No	0.4300	0.25	0.43	3.00	4.07	3	42.0	

In Zone: D											
In Wall:	N ext wall	II - D C - 1	3.7	0.5000	0.20	0.25	2.00	1.07		70.1	
	<ol> <li>North facing windows</li> </ol>	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	$\Box$
In Wall:	W Ext walls										
,	1 West windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Zone: D	U NW 4										
In Wall:	N ext wall	1 II 0 0 A 1									_
	1 North windows,	User Defined	No	0.5000	0.38	0.35	3.00	4.67	5	70.1	
In Wall.	approx. 70 SF W Ext walls										
in wan:	1 West windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Zone: D	U S 2,3 center										
	S Ext wall										
	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	70.1	
In Zone: D											
In Wall:	S ext wall	II - D C - I	NT.	0.4500	0.05	0.42	2.00	1.07	5	70.1	
In Zone: D	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	70.1	$\Box$
	S ext wall										
111 11 11111	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	70.1	
In Zone: D	U SE 1										
In Wall:	E Ext walls										
	1 East windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Wall:	S ext wall			0.4500		0.10			-	<b>70.</b> 4	
	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	70.1	$\Box$
In Zone: D	E Ext walls										
in wan.	1 East windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	
In Wall:	S ext wall				-	0.10					
211 17 1111	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	70.1	
In Zone: D											_
In Wall:	E Ext walls								2		_
1211 52222703	1 East windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	42.0	$\Box$
In Wall:	S ext wall	Han Daffard	N-	0.4500	0.25	0.42	2.00	1.67	-	70.1	
	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	70.1	

In Zone: DU S												
In Wall: Se												
	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	7	70.1	
In Wall: W	est Ext walls											
( Total   13 ( ) ( ) ( ) ( ) ( ) ( )	l West windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	4	42.0	
In Zone: DU S	W 2 3											_
In Wall: Se												
	1 South windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5	-	70.1	
In Wall: W		osci Deilica		0.1500	0.20	0.15	5.00	1.07				ш
	1 West windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3		42.0	
		Oser Defined	110	0.4300	0.25	0.43	5.00	4.07	3		+2.0	ш
In Zone: DU S												
In Wall: Se		Usan Daffar - 1	Nic	0.4500	0.25	0.42	2.00	1.67	=		70.1	
II	<ol> <li>South windows</li> </ol>	User Defined	No	0.4500	0.25	0.43	3.00	4.67	5		70.1	$\Box$
In Wall: W		22 27 27 2	100	2 7277		2.74	725.00	2752227	1		72020	_
	1 West windows	User Defined	No	0.4500	0.25	0.43	3.00	4.67	3	4	42.0	$\Box$
				Doo	ors							
No.	Description	Trons	Shaded?	VVI dela	H (Effec)	Model	Area	Cond.	Done	Heat Cap.	R-Value	7
INO.	Description	Type	Shaded?									No.
				[ft]	[ft]	plier	[sf] [E	tu/nr. st. F	[Ib/ci]	[Btu/sf. F]	[h.sf.F/Btu	ıj
In Zone: DU SW	7.4											
	N entry wall											
In waii:		Steel exterior door	No	3.00	( (7	1.5						
1	entry door to unit		INO				20.0	0.5000	0.00	0.00	2.00	
In Zone: DU SE				5.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
in to to the state of the state	4	ASHRAE App		5.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
		ASHRAE App		5.00	0.07	1	20.0	0.5000	0.00	0.00	2.00	
In Wall:	N entry wall		No									
	N entry wall	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall:	N entry wall entry door to unit		No									
In Wall: 1 In Zone: DU NE	N entry wall entry door to unit	Steel exterior door	No									
In Wall: 1 In Zone: DU NE In Wall:	N entry wall entry door to unit 4 S entry wall	Steel exterior door ASHRAE App		3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: 1 In Zone: DU NE	N entry wall entry door to unit 4 S entry wall	Steel exterior door ASHRAE App Steel exterior door	No No									
In Wall: 1 In Zone: DU NE In Wall: 1	N entry wall entry door to unit 4 S entry wall entry door to unit	Steel exterior door ASHRAE App		3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: 1 In Zone: DU NE In Wall: 1 In Zone: DU NV	N entry wall entry door to unit 4 S entry wall entry door to unit	Steel exterior door ASHRAE App Steel exterior door		3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: 1 In Zone: DU NE In Wall: 1 In Zone: DU NV In Wall:	N entry wall entry door to unit 4 S entry wall entry door to unit V 4 S entry wall	Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No	3.00	6.67 6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: 1 In Zone: DU NE In Wall: 1 In Zone: DU NV	N entry wall entry door to unit 4 S entry wall entry door to unit V 4 S entry wall	Steel exterior door ASHRAE App  Steel exterior door ASHRAE App  Steel exterior door		3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: 1 In Zone: DU NE In Wall: 1 In Zone: DU NV In Wall: 1	N entry wall entry door to unit  4 S entry wall entry door to unit  V 4 S entry wall entry door to unit	Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No	3.00	6.67 6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: 1 In Zone: DU NE In Wall: 1 In Zone: DU NV In Wall: 1 In Zone: DU N o	N entry wall entry door to unit  4 S entry wall entry door to unit  V 4 S entry wall entry door to unit	Steel exterior door ASHRAE App  Steel exterior door ASHRAE App  Steel exterior door	No	3.00	6.67 6.67	1	20.0	0.5000	0.00	0.00	2.00	

	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUSc	enter 4											
	In Wall:	N entry wall											- 1
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DUSW	71	*.*										- 1
		N entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										_
In Zone:	DU SE	1											
	In Wall:	N entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										_
In Zone:	DU NE	1											
		S entry wall											- 1
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DU NV	V 1											
]	In Wall:	S entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DUNG	enter 1											- 1
		S entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DUSc	enter 1											- 1
		N entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DU N 2	2.3 center	**										- 1
		S entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DUS 2	.3 center	**										
		N entry wall											
	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App										
In Zone:	DUSW	7 2,3	resource with the state of the										- 1
	In Wall:	N entry wall											
	1		Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
			ASHRAE App	200000			7.0					70.70	

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T. SV-II. N and an II	In		N entry wall		1000			100		100000000000000000000000000000000000000	rarrarar			

	No Descript	tion Type	U [Btu/hr		C	Vis.Trans	W [ft]	H (Effec) Multiplier [ft]	Area [Sf]	Total Area [Sf]	
			9	Skylight	S						
1	area	roof R-38	0.00	128.00	1	708.0	0.00	0.0270		37.0	
In Zone:		ASHRAE Appendix	6.00	128.00	1	768.0	0.00	0.0270		37.0	
In Zone:		ASHRAE Appendix roof R-38	31.25	64.00	1	2000.0	0.00	0.0270		37.0	
1	roof-ceiling over N center DU	ASHRAE Appendix roof R-38	31.25	67.00	1	2093.8	0.00	0.0270		37.0	
In Zone:	roof-ceiling over NW corner DU	ASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	DU	EASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	Ц
	corner SE DU DU NE 4	roof R-38									_
In Zone:		ASHRAE Appendix	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	DU SW 4	ASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
2	section North facing roof section	plywood roof 5/8"	34.25	131.00	1	4486.8	22.50	0.8137		1.2	
In Zone:	South facing roof	plywood roof 5/8"	34.25	128.00	1	4384.0	22.50	0.8137		1.2	
1	roof over elevator	ASHRAE Appendix roof R-38	12.00	8.00	1	96.0	0.00	0.0270		37.0	Ш

					Floors							
1	No	Description	Туре	Width [ft]	H (Effec) [ft]	Multi plier		Cond. Btu/hr. sf. F]	Heat Cap. [Btu/sf. F]		R-Value [h.sf.F/Btu]	
In Zone:		levator zones	ANY O CONTRACTOR PARAMETERS	Ta Fall (Miles)	24.52777944400	920	20000000	100000000000000000000000000000000000000	400004-00000		THE AMERICA	
1		Slab at bottom of elevator shaft	Soil, concrete slab, carpet/pad	8.00	12.00	1	96.0	0.2725	29.33	110.00	3.67	
In Zone:	A	ttic										
1		attic section overhanging smaller dwelling space	ASHRAE Appendix roof R-38	1.50	68.50	2	102.8	0.0270			37.04	
In Zone:	D	U SW 4										
1		Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U SE 4										
1		Raised floors	R-19 generic floor	32.00	31.25	1	1000.0	0.0526			19.00	
		between units	insulation									
In Zone:	D	U NE 4										
1		Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U NW 4										
1		Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U N center 4										
1		Raised floors between units	R-19 generic floor insulation	31.25	67.00	1	2093.8	0.0526			19.00	
In Zone:	D	U S center 4										
1		Raised floors between units	R-19 generic floor insulation	31.25	64.00	1	2000.0	0.0526			19.00	
In Zone:	D	U SW 1										
1		Slab floor	Soil, concrete slab, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	D	U SE 1	400 m (400 m) (400 m) (400 m)									
1		Bottom floor slab	Soil, concrete slab, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	D	U NE 1	1000 A 10 St 4 7777									
1		Bottom floor slab	Soil, concrete slab, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	D	U NW 1										

1	Bottom floor slab	Soil, concrete slab, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU N center 1	carper pau									
1	Slab floor	Soil, concrete slab, carpet/pad	31.25	67.00	1	2093.8	0.2725	29.33	110.00	3.67	
In Zone:	DU S center 1										
1	Slab floor	Soil, concrete slab, carpet/pad	31.25	64.00	1	2000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU N 2,3 center										200
1	raised floor between units	R-19 generic floor insulation	31.25	67.00	1	2093.8	0.0526			19.00	
In Zone:	DUS 2,3 center										-
1	raised floor	R-19 generic floor insulation	31.25	64.00	1	2000.0	0.0526			19.00	
In Zone:	DU SW 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU SE 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU NW 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU NE 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	Cor 4										
1	Floor in corridor space of 4th floor	R-19 generic floor insulation	6.00	128.00	1	768.0	0.0526			19.00	
In Zone:	Cor 1										
1	slab in corridor space	Soil, concrete slab, carpet/pad	6.00	128.00	1	768.0	0.2725	29.33	110.00	3.67	
In Zone:	Cor 2,3										
1	Raised floor in corridor spaces	R-19 generic floor insulation	6.00	128.00	1	768.0	0.0526			19.00	

## Systems

HP SW 4	heat pump	Constant System < 6	No. Of Units 1				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SE 4	Heat pump	Constant System < 6	Split	No. Of Units 1			
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NE 4	heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NW 4	Heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System					$\overline{}$	

HP NC 4	Heat pump	Constant System < 0	No. Of Units 2				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SC 4	Heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SW 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750,00	0.50				
4	Air Distribution System						
HP SE 1	Heat pump	Constant System < 6	No. Of Units 1				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System					$\overline{\Box}$	

HP NE 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NW 1	Heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NC 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SC 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	18000.00	7.40				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						

HP N2,3 C	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 4	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP S 2,3 C	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 4	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP SW 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP SE 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					$\overline{\Box}$

HP NW 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	ory Capacity Eff				
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NE 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			$\overline{}$
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System		***			
HP Corr 4	Heat pump thru wall	Through the Single Pac	he wall AirConditi kage	oner	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60			
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			
HP Coor 1	HP thru wall	Through the Single Pac	he wall AirConditi kage	oner	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60			
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			

HP Corr.2,3	HP thru wall	Through the Single Pac	oner	No. Of Units 4		
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60			
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			

		Plant			
Equipment	Category	Size	Inst.No	Eff.	IPLV

	Wat	er Heaters			
W-Heater Description	CapacityCap.Unit	I/P Rt.	Efficiency	Loss	
1 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
2 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
3 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
4 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	[
5 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	[
6 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	1
7 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
8 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	į
9 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
10 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
11 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
12 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
13 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
14 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
15 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	ĺ
16 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	j
17 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	i
18 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	i
19 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	j

O Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
21 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
22 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
23 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
24 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
25 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
26 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
27 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
28 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
29 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
30 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
31 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
32 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]

Ext-Lighting										
Description	Category	No. of Luminaires	Watts per Luminaire	Area/Len/No. of units [sf/ft/No]	Control Type	Wattage [W]				
		Piping	g							
No Type		Operating Temperature [F]	Insulation Conductivity [ Btu-in/h.sf.H		Insulation Thickness [in]	Is Runout?				
							_			

			Fenestra	ation Used			
Name	Glass Type	No. of Panes	Glass Conductance [Btu/h.sf.F]	SHGC	VLT		

Base N Atl window	User Defined	2	0.5000	0.3800	0.3500	
Base other Atl window	User Defined	2	0.4500	0.2500	0.4300	

	Materials Used								
Mat No	Acronym	Description	Only R-Value Used	RValue [h.sf.F/Btu]	Thickness [ft]	Conductivity [Btu/h.ft.F]	Density [lb/cf]	SpecificHeat [Btu/lb.F]	
151	Matl151	CONC HW, DRD, 140LB, 4IN	No	0.4403	0.3333	0.7570	140.00	0.2000	
178 1015	Matl178 ApLbMatl015	CARPET W/RUBBER PAD Soil, 1 ft	Yes No	1.2300 2.0000	1.0000	0.5000	100.00	0.2000	

			(	Cons	structs	Used					
No	Name		Sim Const	•	Massless Construct	Conductar [Btu/h.sf.]		nt Capacity Btu/sf.F]	Density [lb/cf]	RValue [h.sf.F/Btu]	
1062	R-13 wall 16 OC	Ashrae App	No.	0	Yes	0.09				11.2	
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor				
	1	1013	R-13 wall 16 OC ASHRA	E App.			0.000				
No	Name		Sim Const		Massless Construct	Conductar [Btu/h.sf.]		nt Capacity Btu/sf.F]	Density [lb/cf]	RValue [h.sf.F/Btu]	
1063	Steel exterior do	or ASHRAE	App No	0	Yes	0.50				2.0	
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor				
	1	288	Steel exterior door ASHR.	AE App			0.000				

No	Name			Simple Construct	Massless Construct		[TTT]		RValue [h.sf.F/Btu]	
1064	Soil, concrete sl	ab, carpet/pa	d	No	No	0.27	29.33	110.00	3.7	
	Layer	Material No.	Material			Thickness [ft]	Framing Factor			
	1	1015	Soil, 1 ft			1.0000	0.000			
	2	151	CONC HW, DRD,	140LB, 4IN		0.3333	0.000			
	3	178	CARPET W/RUBE	BER PAD			0.000			
No	Name			Simple Construct	Massless Construct				RValue [h.sf.F/Btu]	
1068	plywood roof 5/	8"		No	Yes	0.81			1.2	
-	Layer	Material No.	Material			Thickness [ft]	Framing Factor			
	1	1010	PLYWOOD, 5/8IN			0.0521	0.000			
	2	1011	ASPHALT-SHING	LE AND SID	ING	0.0200	0.000			
No	Name			Simple Construct	Massless Construct				RValue [h.sf.F/Btu]	
1069	Attic gable end	wall		No	Yes	1.58			0.6	
	Layer	Material No.	Material			Thickness [ft]	Framing Factor			
	1	244	PLYWOOD, 1/2IN			0.0417	0.000			

No	Name			Simple Construct	Massless Construct	Conducta [Btu/h.sf.		Density [lb/cf]	RValue [h.sf.F/Btu]	
1070	ASHRAE Apper	ndix roof R-3	38	No	Yes	0.03			37.0	
	Layer	Material No.	Material		Ti	hickness [ft]	Framing Factor			
	1	1012	R-38 roof truss A	SHRAE App.			0.000			
No	Name			Simple Construct	Massless Construct	Conducta [Btu/h.sf.		Density [lb/cf]	RValue [h.sf.F/Btu]	
1071	R-19 generic flo	or insulation		No	Yes	0.05			19.0	
	Layer	Material No.	Material		T	hickness [ft]	Framing Factor			
	1	1014	R-19 Generic Inst	ulation	C	0.4147	0.000			

## CHICAGO

## EnergyGauge Summit v3.11 INPUT DATA REPORT

## **Project Information**

Project Name: Baseline MF Chicago Orientation: North

Project Title: Code minimum apartment in Chicago Building Type: Multi-Family

Address: Enter Address here Building Classification: New Finished building

Enter Address here

State: Illinois No.of Storeys: 4

Zip: 0 GrossArea: 44517 SF

Owner: NMHC

			Zones				
No	Acronym	Description	Туре	Area [sf]	Multiplier	Total Area [sf]	
1	Elevator zones	Elevator areas with mechanical space	UNCONDITIONED	96.0	1	96.0	
2	Attic	Attic	UNCONDITIONED	8973.5	1	8973.5	
3	DU SW 4	Dwelling unit SW corner on 4th story	CONDITIONED	1000.0	1	1000.0	
4	DU SE 4	Dwelling unit SE corner on 4th story	CONDITIONED	1000.0	1	1000.0	

5	DU NE 4	Dwelling unit on 4th floor at NE corner	CONDITIONED	1000.0	1	1000.0	
6	DU NW 4	Dwelling unit on 4th floor	CONDITIONED	1000.0	1	1000.0	
7	DUN center 4	at NW corner North DUs on 4th floor in	CONDITIONED	2093.8	1	2093.8	
		center					100-00
8	DU S center 4	South DUs on 4th floor in center	CONDITIONED	2000.0	1	2000.0	
9	DU SW 1	Dwelling unit SW corner on 1st story	CONDITIONED	1000.0	1	1000.0	
10	DU SE 1	Dwelling unit SE corner	CONDITIONED	1000.0	1	1000.0	
11	DU NE 1	on 1st story Dwelling unit on 1st floor at NE corner	CONDITIONED	1000.0	1	1000.0	
12	DU NW 1	Dwelling unit on 1st floor at NW corner	CONDITIONED	1000.0	1	1000.0	
13	DU N center 1	North DUs on 1st floor in center	CONDITIONED	2093.8	1	2093.8	
14	DU S center 1	South DUs on 1st floor in center	CONDITIONED	2000.0	1	2000.0	
15	DU N 2,3 center	Interior North DUs on 2nd and 3rd floors	CONDITIONED	4187.5	1	4187.5	
16	DU S 2,3 center	Interior south DUs on 2nd and 3rd floors	CONDITIONED	4000.0	1	4000.0	
17	DU SW 2,3	Dwelling unit SW corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
18	DU SE 2,3	Dwelling unit SE corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
19	DU NW 2,3	Dwelling unit NW corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
20	DU NE 2,3	Dwelling unit NE corner	CONDITIONED	2000.0	1	2000.0	
21	Cor 4	on 2nd and 3rd story 4th floor corridor	CONDITIONED	768.0	1	768.0	
22	Cor 1	1st floor corridor	CONDITIONED	768.0	1	768.0	
23	Cor 2,3	2nd, 3rd floor corridors	CONDITIONED	1536.0	1	1536.0	

			S	paces						
No	Acronym	Description	Туре	Depth [ft]	Width [ft]	Height [ft]	Multi plier	Total Area [sf]	Total Volume [cf]	-
In Zone		combined elevator and	Electrical Mechanical Equipment Room - General	8.00	12.00	35.00	1	96.0	3360.0	
In Zone	: Attic attic space	attic space with average height assumed	Storage & Warehouse - Inactive Storage	68.50	131.00	8.50	1	8973.5	76274.8	
In Zone		individual dwelling unit	Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0	
In Zone	: DU SE 4 DU SE 4		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008	
In Zone	: DU NE 4 DU NE 4		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008	
In Zone	DU NW 4		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008	
In Zone			Private Living Space	31.25	33.50	8.00	2	2093.8	16750.0	
In Zone			Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	: DU SW 1 DU SE 1		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008	
In Zone	: DU SE 1 DU SE 1	The second second	Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008	
In Zone	: DU NE 1 DU NE 1	DU on NE corner of 1st	Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008	
In Zone	: DU NW DU NW 1	story  1  DU on NW corner of 1st story	Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0	

In Zone										24-03
1	DU N center	DU north in center of	Private Living Space	31.25	33.50	8.00	2	2093.8	16750.0	
In Zone	: DU S cer	lst story								
		DU south in center of	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	П
		1st story	Titale Bring space		02.00					_
In Zone										<u> </u>
1	DU interior N	oDUs in interior of 2nd	Private Living Space	31.25	33.50	8.00	4	4187.5	33500.0	
	DUGGG	and 3rd follrs								
In Zone			Private Living Space	31.25	32.00	8.00	4	4000.0	32000.0	П
	Do center soc	3rd floors	Tivate Living Space	31.23	32.00	0.00	7	4000.0	32000.0	ш
In Zone	: DU SW									
1	DU SW 2,3	individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	: DU SE 2	.3								
	DU SE 2,3	individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	: DU NW	23								_
		individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone		č	0 1							_
	DU NE 2,3	بى individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
		man idair aweining and	Tivate Biving Space	51.25	52.00	0.00	L	2000.0	10000.0	ш
In Zone	c: Cor 4 Corridor 4	Corridor space on 4th	Carridae	128.00	6.00	8.00	1	768.0	6144.0	
1	Corridor 4	floor	Corridor	128.00	0.00	8.00	1	708.U	0144.0	ш
In Zone	e: Cor 1	HOVE								
1		e.Corridor space	Corridor	128.00	6.00	8.00	1	768.0	6144.0	
In Zone	: Cor 2,3	6%								
	Corr 2,3	Corridor space 2,3	Corridor	128.00	6.00	8.00	2	1536.0	12288.0	
		floors		.m. 75.50.50.50.1	2100		~			_

	Lighting									
1	No	Туре	Category	No. of Luminaires	Watts per Luminaire	Power [W]	Control Type	No.of Ctrl pts		
In Zone: Ele In Space:	vator z elevat 1		General Lighting	1	144	144	Manual On/Off	1		

In Zone: Att	ic								
In Space:		space Incandescent	General Lighting	35	75	2625	Manual On/Off	4	
In Zone: DU In Space:	SW 4	F Poof							
In Space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	SE 4	F.4							
In Space:	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	NE 4								
In Space:	DU N	E 4 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	NW 4								<del></del> 0
In Space:	DU N	W 4 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N cen		General Eighang	J	00	500	Ividited Of Off		ш
In Space:	DU N	center 4	0 11:1:	10	10	224	10 00		_
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	S cent								
3/85	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	SW 1	F 1							
In Space:	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	SE 1								36—33
In Space:	DU S	E 1 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	

	72	53: 5:	2 3233		120				
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	NE 1	oleven)							
In Space:	DU N	E 1 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	Principle of the Control of the Cont	6	7.5				
	-3.0		General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NW 1								
m space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N cen	ter 1							
In Space:		center 1 Compact Fluorescent	Consed Lighting	18	18	324	Manual On/Off		
	1		General Lighting					1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	S cent	ter 1 center bottom							
in space:	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N 2,3	center							
In Space:	DU in	nterior North							
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
		center							
In Space:	DU co	enter south Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	-77.0		General Lighting	O	00	300	Manual Off Off	1	
In Zone: DU In Space:	SW 2								
m space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	SE 2,3	3							
In Space:	DU S	E 2,3		1947		1227	100 100 000		
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	

In Zone: DU In Space:	NW:								
in opiite.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NE 2 DU I								
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: Con	r 4								
In Space:	Corr								
	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	
In Zone: Con	r 1								
In Space:	Corr	ridor spaces							
0-00001 <del>1</del> .00000000	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	
In Zone: Con	2,3								
In Space:	Corr	2,3							
2 x 22 x 9 x 20 x 2 x 2 x 2 x 2 x 2 x 2 x 2 x 2 x	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	

					Walls						
No	Description	Туре	Width I [ft]	H (Effec) [ft]	Multi plier	Area [sf]		Conductance [Btu/hr. sf. F]	Heat Capacity [Btu/sf.F]	Dens. R-Valu [lb/cf] [h.sf.F/E	
In Z	Cone: Elevator zone	s									
1	East facing elevator wall 1st floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	East	0.0890		11.2	2 🗆
2	East facing elevator wall 2,3 floor	R-13 wall 16 OC Ashrae App	12.00	8.00	2	96.0	East	0.0890		11.2	
3	East facing elevator wall 4th floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	East	0.0890		11.2	
4	West facing elevator wall 1st floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	West	0.0890		11.2	
5	West facing elevator wall 2,3 floor	R-13 wall 16 OC Ashrae App	12.00	8.00	2	96.0	West	0.0890		11.2	

6	West facing elevator wall	R-13 wall 16 OC	12.00	8.00	1	96.0	West	0.0890	11.2	
7	4th floor North facing elevator	Ashrae App R-13 wall 16 OC	8.00	8.00	1	64.0	North	0.0890	11.2	
	wall 1st floor	Ashrae App								(2)
8	North facing elevator	R-13 wall 16 OC	8.00	8.00	2	64.0	North	0.0890	11.2	
	wall 2,3 floors	Ashrae App					20.00	2000		_
9	North facing elevator wall 4th floor	R-13 wall 16 OC Ashrae App	8.00	8.00	1	64.0	North	0.0890	11.2	
In Z		Asiliac App								
1	Attic gable end wall	Attic gable end wall	68.50	8.56	1	586.4	East	1.5827	0.6	
1	facing east	Attic gable end wan	06.50	6.30	1	300.4	East	1.3621	0.0	
2	Attic gable end wall	Attic gable end wall	68.50	8.56	1	586.4	West	1.5827	0.6	
7.000	facing west									
In Z										
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
1.5	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
		Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
In Z	one: DU SE 4	••								
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
0.000		Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
800	corridor	Ashrae App								
In Z	one: DU NE 4									
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	corridor	Ashrae App							,-,-,-,-	_
In Z										
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	walls	Ashrae App	22100	0.00		200.0	_10141	( managed and		_
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
_	walls	Ashrae App		****	- T		11.404	INDIANA.		_
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	corridor	Ashrae App	J 2.00	0.00		200.0	Journ	5,505.5	11.2	_
	COTTIGOT	тынастрр								

In Z	one: DU N center 4	9								
1	North facing exterior	R-13 wall 16 OC	33.50	8.00	2	268.0	North	0.0890	11.2	
	walls	Ashrae App								
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
500	between units	Ashrae App								_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
	between units	Ashrae App	40000400	12122	100	2002000			National Control	
4	Wall between unit and	R-13 wall 16 OC	33.50	8.00	2	268.0	South	0.0890	11.2	
	corridor	Ashrae App								
2000000000	one: DUS center 4		22.00	0.00		2560	G .1	6 6000		
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
3	East facing walls	Ashrae App R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
3	East facing wans	Ashrae App	31.23	0.00	1	230.0	East	0.0690	11.2	_
4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.2	П
	corridor	Ashrae App	2.00		-	200.0	2.02.02			_
In Z	W7.557.05950									
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App								
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
	walls	Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
In Z		D 10 1114600								_
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App	21.05	9.00	1	250.0	T	0.0890	11.0	
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	1	250.0	East	0.0890	11.2	ш
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
J	corridor	Ashrae App	32.00	0.00	1	250.0	Ivorui	0.0090	11.2	ш
In Z		, made , spp								
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	walls	Ashrae App	52.00			200.0	1101111	0.000	11.2	_
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								_
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
100	corridor	Ashrae App								
In Z	one: DU NW 1									

1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256,0	North	0.0890	11	2	$\Box$
1	walls	Ashrae App	32.00	0.00	1	250.0	ivolui	0.0070	11	. 2	_
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	2	
170	walls	Ashrae App									
3	Wall between unit and	R-13 wall 16 OC	8.00	32.00	1	256.0	South	0.0890	11	.2	
	corridor	Ashrae App									_
In 2	Zone: DU N center	1									
1	North facing exterior	R-13 wall 16 OC	33.50	8.00	2	268.0	North	0.0890	11	2	
	walls	Ashrae App									
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
	between units	Ashrae App									
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11	.2	
	between units	Ashrae App									
4	Wall between unit and	R-13 wall 16 OC	27.50	8.00	2	220.0	South	0.0890	11	.2	
	corridor	Ashrae App									1.32
In Z	Zone: DU S center 1										
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11	.2	
	walls	Ashrae App									_
2	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11	.2	
- 62	between units	Ashrae App	0.000								_
3	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
	between units	Ashrae App	230022	12022	1020	22200		1012200		020	_
4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11	.2	
I	corridor	Ashrae App									
100	Cone: DU N 2,3 cen		22.50	0.00		250.0		0.0000			-1
1	North walls on interior	R-13 wall 16 OC	33.50	8.00	4	268.0	North	0.0890	11	.2	
	DUs	Ashrae App	21.25	0.00	•	250.0		0.0000		•	-
2	East facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11	. 2	
,	between units	Ashrae App	21.05	8.00	2	250.0	West	0.0000	11	^	
3	West facing walls between units	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	west	0.0890	11	. 2	ᄓ
4	Wall between unit and	R-13 wall 16 OC	27.50	8.00	4	220.0	South	0.0890	11	2	
4	corridor	Ashrae App	27.50	8.00	4	220.0	South	0.0690	11	. 4	ᄓ
In 2	Cone: DU S 2,3 cent										
1	North walls on interior	R-13 wall 16 OC	33.50	8.00	4	268.0	South	0.0890	11	2	
	DUs	Ashrae App	33.50	0.00	7	200.0	Doddi	0.0070	11		_
2	West facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	West	0.0890	11	2	
	rrest facilig walls	Ashrae App	31.23	0.00	2	250.0	VYVSU	0.0070	11	-	_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11	2	
	Trans taking wans	Ashrae App	01.20	0.00	2	250.0	1.74.50	0.0070	11	. 2	_
		. made rapp									

4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	4	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
In Z									****	
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	West	0.0890	11.2	
3	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
In Z		. wilde . ipp								
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11.2	
3	Wall between unit and corridor	Ashrae App R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
In 7		Asnrae App								
In Z	one: DU NW 2,3  North facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.2	
1	walls	Ashrae App			2					
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	West	0.0890	11.2	
3	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
In Z	one: DU NE 2,3									
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	East	0.0890	11.2	
3	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
In Z	one: Cor 4									50
1	corridor end wall facing east	R-13 wall 16 OC Ashrae App	6.00	8.00	1	48.0	East	0.0890	11.2	
2	Corridor wall facing west	R-13 wall 16 OC Ashrae App	6.00	8.00	1	48.0	West	0.0890	11.2	
In Z	one: Cor 1	rishi de ripp								
1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	1	48.0	East	0.0890	11.2	
2	east Corridor wall facing west	Ashrae App R-13 wall 16 OC	6.00	8.00	1	48.0	West	0.0890	11.2	
In Z	one: Cor 2,3	Ashrae App								

1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	2	48.0	East	0.0890	11.2	
2	east Corridor wall facing west	Ashrae App R-13 wall 16 OC Ashrae App	6.00	8.00	2	48.0	West	0.0890	11.2	

					Windo	ws								
	No	Description	Туре	Shaded	U [Btu/hr sf F]	SHGC	Vis.Tra	W [ft]	H (Effec) [ft]	Multi plier	Total Area [sf]			
In Zone: DU N 2,3 center In Wall: N Ext wall														
in wan:	N EX	North windows	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1			
In Zone: DU	J N ce	enter 1												
In Wall:	N ext											_		
	1	North windows	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1			
In Zone: DU														
In Wall:	N ext	wall North windows	User Defined	No	0,4800	0.49	0.52	3.00	4.67	5	70.1			
In Zone: DU			Oser Defined	110	0.4600	0.49	0.52	3.00	4.07	3	70.1	ш		
In Wall:														
	1	East windows,	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0			
In Wall:	N ext	wall												
	1	North windows,	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1			
In Zone: DU												-		
In Wall:							11011000	100000000000000000000000000000000000000	700000000		No. 400 400	_		
		East windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0			
In Wall:			TT D C 1		0.4000	0.40	0.52	2.00	4.67	~	70.1			
	1	North windows	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1			
In Zone: DU In Wall:		A												
III wan.	E EXC	West windows,	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0			
		approx. 280 SF	Oser Defined	110	0.5 100	0.51	0.50	5.00	1.07		12.0			
In Wall:	N ext	wall												
	1	North windows	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1			
In Zone: DU		T												
In Wall:			II D.C.		0.4000	0.40	0.50	2.00	1.67	-	70.1			
* ***	1	North windows	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1			
In Wall:	W Ex	t walls East windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0			
	1	East windows	Oser Defined	INO	0.3400	0.34	0.50	5.00	4.07	3	42.0			

In Zone: DU NW 2,3										
In Wall: N ext wall		1994		102004020				110	222	_
<ol> <li>North facing</li> </ol>	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1	
windows										
In Wall: W Ext walls  1 West windows,	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0	
In Zone: DU NW 4	Oser Defined	140	0.3400	0.34	0.50	3.00	4.07	3	42.0	$\Box$
In Wall: N ext wall										
1 North windows,	User Defined	No	0.4800	0.49	0.52	3.00	4.67	5	70.1	
approx. 70 SF	CSCI Dellied	110	0.4000	0.42	0.52	5.00	4.07	5	70.1	
In Wall: W Ext walls										
1 West windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0	
In Zone: DUS 2,3 center										_
In Wall: S Ext wall										
<ol> <li>South windows</li> </ol>	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	70.1	
In Zone: DU S center 1										
In Wall: S ext wall	H D C 1		0.0400	0.04	0.56	2.00	4.60	16	70.1	
1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	70.1	$\Box$
In Zone: DUS center 4										
In Wall: S ext wall 1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	70.1	
In Zone: DU SE 1	Osci Defined	140	0.5400	0.54	0.50	5.00	4.07	- 2	70.1	ᆜ
In Wall: E Ext walls										
1 East windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0	
In Wall: S ext wall								_		
1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	70.1	
In Zone: DU SE 2,3										
In Wall: E Ext walls										
1 East windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0	
In Wall: S ext wall										
<ol> <li>South windows</li> </ol>	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	70.1	
In Zone: DU SE 4										
In Wall: E Ext walls	D.c. :		0.0406	0.04	0.56	2.00			12.0	
1 East windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	42.0	
In Wall: S ext wall	H D C .		0.0100	0.24	0.56	2.00	1.67	_	70.1	
1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	70.1	

In Zone: DU												
In Wall:			1994						119	112		_
	1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	7	0.1	L
In Wall:	W Ext walls						000000000000000000000000000000000000000					_
	1 West windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	- 4	2.0	L
In Zone: DU												
In Wall:												
	1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	7	0.1	
In Wall:	W ext walls											
	<ol> <li>West windows approx. 280 SF</li> </ol>		No	0.3400	0.34	0.56	3.00	4.67	3	- 4	2.0	
In Zone: DU	SW 4											
In Wall:	S ext wall											
	1 South windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	5	7	0.1	Г
In Wall:	W Ext walls											
	1 West windows	User Defined	No	0.3400	0.34	0.56	3.00	4.67	3	4	2.0	Г
				Doo	rs							
N	D i et	т	CL - J - J9	***************************************	II (Eff)	M-14:		C1	D	H4-C	D.VI	
No	Description	Туре	Shaded?	***************************************	H (Effec)	Multi plier	Area [sf] [I	Cond. Btu/hr. sf. F]		Heat Cap. [Btu/sf. F]	R-Value	
	•	Туре	Shaded?	Width								
In Zone: DU S	W 4	Туре	Shaded?	Width								
In Zone: DU S In Wall	W 4 N entry wall	2000	2000	Width [ft]	[ft]	plier	[sf] [I	Btu/hr. sf. F]	[lb/cf]	[Btu/sf. F]	[h.sf.F/Bt	
In Zone: DU S In Wall	W 4 N entry wall	Steel exterior door	Shaded?	Width								
In Zone: DU S In Wall	W 4  N entry wall entry door to unit	2000	2000	Width [ft]	[ft]	plier	[sf] [I	Btu/hr. sf. F]	[lb/cf]	[Btu/sf. F]	[h.sf.F/Bt	
In Zone: DU S In Wall In Zone: DU S	W 4  N entry wall entry door to unit	Steel exterior door	2000	Width [ft]	[ft]	plier	[sf] [I	Btu/hr. sf. F]	[lb/cf]	[Btu/sf. F]	[h.sf.F/Bt	
In Zone: DU S In Wall In Zone: DU S In Wall	W 4  • N entry wall  • entry door to unit  E 4  • N entry wall	Steel exterior door ASHRAE App	No	Width [ft]	[ft] 6.67	plier 1	[sf] [I	0.5000	(lb/cf]	(Btu/sf. F)	[h.sf.F/Bt	
In Zone: DU S In Wall In Zone: DU S In Wall	W 4  • N entry wall  • entry door to unit  E 4  • N entry wall	Steel exterior door ASHRAE App	2000	Width [ft]	[ft]	plier	[sf] [I	Btu/hr. sf. F]	[lb/cf]	[Btu/sf. F]	[h.sf.F/Bt	
in Zone: DU S In Wall In Zone: DU S In Wall	W 4  N entry wall entry door to unit  E 4  N entry wall entry door to unit	Steel exterior door ASHRAE App	No	Width [ft]	[ft] 6.67	plier 1	[sf] [I	0.5000	(lb/cf]	(Btu/sf. F)	[h.sf.F/Bt	
In Zone: DU S In Wall In Zone: DU S In Wall In Cone: DU S	W 4  N entry wall entry door to unit E 4  N entry wall entry door to unit	Steel exterior door ASHRAE App	No	Width [ft]	[ft] 6.67	plier 1	[sf] [I	0.5000	(lb/cf]	(Btu/sf. F)	[h.sf.F/Bt	
In Zone: DU S In Wall In Zone: DU S In Wall In Zone: DU N In Zone: DU N	W 4  : N entry wall entry door to unit  E 4  : N entry wall entry door to unit  E 4  : S entry wall	Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No No	Width [ft] 3.00	6.67 6.67	plier  1	20.0 20.0	0.5000 0.5000	0.00 0.00	0.00 0.00	2.00 2.00	
In Zone: DU S In Wall In Zone: DU S In Wall In Zone: DU N In Zone: DU N	W 4  : N entry wall entry door to unit  E 4  : N entry wall entry door to unit  E 4  : S entry wall	Steel exterior door ASHRAE App Steel exterior door ASHRAE App Steel exterior door	No	Width [ft]	[ft] 6.67	plier 1	[sf] [I	0.5000	(lb/cf]	(Btu/sf. F)	[h.sf.F/Bt	
in Zone: DU S In Wall in Zone: DU S In Wall in Zone: DU N In Wall	W 4  N entry wall entry door to unit E 4 N entry wall entry door to unit S 4 S entry wall entry door to unit	Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No No	Width [ft] 3.00	6.67 6.67	plier  1	20.0 20.0	0.5000 0.5000	0.00 0.00	0.00 0.00	2.00 2.00	
In Zone: DU S In Wall In Zone: DU S In Wall In Zone: DU N In Wall In Wall In Zone: DU N	W 4  N entry wall entry door to unit E 4 N entry wall entry door to unit S 4 S entry wall entry door to unit	Steel exterior door ASHRAE App Steel exterior door ASHRAE App Steel exterior door	No No	Width [ft] 3.00	6.67 6.67	plier  1	20.0 20.0	0.5000 0.5000	0.00 0.00	0.00 0.00	2.00 2.00	
in Zone: DU S In Wall in Zone: DU S In Wall in Zone: DU N In Wall in Zone: DU N In Wall	W 4  N entry wall entry door to unit  E 4  N entry wall entry door to unit  E 4  S entry wall entry door to unit  W 4  S entry wall  S entry wall	Steel exterior door ASHRAE App Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No No	Width [ft]  3.00  3.00  3.00	6.67 6.67	plier  1  1	20.0 20.0 20.0	0.5000 0.5000 0.5000	0.00 0.00 0.00	0.00 0.00 0.00	2.00 2.00 2.00	
in Zone: DU S In Wall in Zone: DU S In Wall in Zone: DU N In Wall in Zone: DU N In Wall	W 4  N entry wall entry door to unit E 4 N entry wall entry door to unit S 4 S entry wall entry door to unit	Steel exterior door ASHRAE App Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No No	Width [ft] 3.00	6.67 6.67	plier  1	20.0 20.0	0.5000 0.5000	0.00 0.00	0.00 0.00	2.00 2.00	
in Zone: DU S In Wall in Zone: DU S In Wall in Zone: DU N In Wall in Zone: DU N In Wall	W 4  N entry wall entry door to unit  E 4  N entry wall entry door to unit  E 4  S entry wall entry door to unit  W 4  S entry wall entry door to unit  W 4  S entry wall entry door to unit	Steel exterior door ASHRAE App Steel exterior door ASHRAE App Steel exterior door ASHRAE App	No No	Width [ft]  3.00  3.00  3.00	6.67 6.67	plier  1  1	20.0 20.0 20.0	0.5000 0.5000 0.5000	0.00 0.00 0.00	0.00 0.00 0.00	2.00 2.00 2.00	

In Zone: DU N center 4 In Wall: S entry wall

	1	entry door to unit	Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
2 222			ASHRAE App										
In Zone:													
I	n Wall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUSW	1	Tr										
	n Wall:	N entry wall											
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU SE	1											
I	n Wall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU NE	1											
I	n Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU NW	7 1											
I	n Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU N e	enter 1											
	n Wall:												
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUSc	enter 1	• •										
I	n Wall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:			10 mm 1 m										
I	n Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUS 2	3 center	**										
		N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUSW	2.3											
	n Wall:												
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	

In Wall:   Nentry wall   1   entry door to unit   Steel exterior door   No   3.00   6.67   1   20.0   0.5000   0.00   0.00   2.00   C	N	lo De	escription T	ype	Width [ft]	H (Effec) [ft]	Multi plier	Area [sf]	Tilt [deg] [E	Cond. Stu/hr. Sf. F]	Heat Cap [Btu/sf. F]		R-Value [h.sf.F/Btu]	
1 entry door to unit						Roo	fs							
1 entry door to unit Steel exterior door ASHRAE App  n Zone: DU NW 2,3 In Wall: S entry wall 1 entry door to unit Steel exterior door ASHRAE App  n Zone: DU NE 2,3 In Wall: S entry wall 1 entry door to unit Steel exterior door ASHRAE App  n Zone: DU NE 2,3 In Wall: S entry wall 1 entry door to unit Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: DU NE 2,3 In Wall: S entry wall 1 entry door to unit Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 4 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 1 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 1 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 1 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 2,3 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 2,3 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 2,3 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □  n Zone: Cor 2,3 In Wall: W corr end  No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 □		1	West stairway doc		No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
1 entry door to unit Steel exterior door ASHRAE App  n Zone: DU NW 2,3 In Wall: Sentry wall 1 entry door to unit Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  n Zone: DU NE 2,3 In Wall: Sentry wall 1 entry door to unit Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  n Zone: Cor 4 In Wall: E corr end 1 East stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 West stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 E corr end 1 E corr end 1 E corr end 1 E sat stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 E corr end 1 E corr end 1 E sat stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 E corr end 1 E sat stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 E corr end 1 E sat stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: E corr end 1 West stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: E corr end 1 E corr end 1 E sat stairway doo: Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App	In	wall:		**										
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1 entry door to unit Steel exterior door ASHRAE App  n Zone: DU NW 2,3 In Wall: Sentry wall 1 entry door to unit Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  n Zone: DU NE 2,3 In Wall: Sentry wall 1 entry door to unit Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  n Zone: Cor 4 In Wall: E corr end 1 East stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 West stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 East stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 East stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 East stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 West stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 West stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 2.00 C ASHRAE App  In Wall: W corr end 1 West stairway door Steel exterior door No 3.00 6.67 1 20.0 0.5000 0.00 0.00 0.00 2.00 C ASHRAE App														
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					No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	L
	In							2	***					-

In Zone:	estadores si = Parecas (Casta Casta Maria	ANA TO TOO TO SEE SEE SEE SEE SEE SEE SEE SEE SEE SE	[Btu/h	r sf F]		www.neder-documentatics.com	[ft]	[ft]	[Sf]	[Sf]	
	No Descript	ion Type	τ	Skylight SHO	1000	Vis.Trans	W	H (Effec) Multiplier	Area	Total Area	
				61 II I							
1	Roof over corridor area	ASHRAE Appendix roof R-38	6.00	128.00	1	768.0	0.00	0.0270		37.0	
In Zone:	Cor 4										4 <u>0 - 20</u>
In Zone:		ASHRAE Appendix roof R-38	31.25	64.00	1	2000.0	0.00	0.0270		37.0	
1	roof-ceiling over N center DU	ASHRAE Appendix roof R-38	31.25	67.00	1	2093.8	0.00	0.0270		37.0	
1 In Zone:	NW corner DU	ASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:			100000			1905/16/21:70**	97907				_
In Zone:	DU NE 4 roof-ceiling over NI DU	EASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
1	roof-ceiling over corner SE DU	ASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	SW corner DU DU SE 4	roof R-38									
In Zone:	section DU SW 4 roof-ceiling over	ASHRAE Appendix	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
2	-	plywood roof 5/8"	34.25	131.00	1	4486.8	22.50	0.8137		1.2	
In Zone:	South facing roof	plywood roof 5/8"	34.25	128.00	1	4384.0	22.50	0.8137		1.2	
1	roof over elevator	ASHRAE Appendix roof R-38	12.00	8.00	1	96.0	0.00	0.0270		37.0	Ш

					Floors							
1	No	Description	Туре	Width [ft]	H (Effec) [ft]	Multi plier		Cond. stu/hr. sf. F]	Heat Cap. [Btu/sf. F]		R-Value [h.sf.F/Btu]	
In Zone:		Clevator zones Slab at bottom of	Soil, Concrete,	8.00	12.00	1	96.0	0.2725	29.33	110.00	3.67	
		elevator shaft	carpet/pad									- T
In Zone:	A	Attic										
1		attic section overhanging smaller dwelling space	ASHRAE Appendix roof R-38	1.50	68.50	2	102.8	0.0270			37.04	
In Zone:	D	OU SW 4										
1	L	Raised floors	R-19 generic floor	32.00	31.25	1	1000.0	0.0526			19.00	
		between units	insulation									
In Zone:			905 (VA 50 cm)									_
1	L	Raised floors	R-19 generic floor	32.00	31.25	1	1000.0	0.0526			19.00	
		between units	insulation									
In Zone:		OU NE 4	D 10 ' 0	22.00	21.25	2	1000 0	0.0525			10.00	
1		Raised floors	R-19 generic floor	32.00	31.25	1	1000.0	0.0526			19.00	
т 7		between units	insulation									
In Zone:	-	DU NW 4 Raised floors	R-19 generic floor	32.00	31.25	1	1000.0	0.0526			19.00	
1		between units	insulation	32.00	31.23	1	1000.0	0.0320			19.00	ш
In Zono:	т	OU N center 4	msulation									
111 Zone.		Raised floors	R-19 generic floor	31.25	67.00	1	2093.8	0.0526			19.00	
		between units	insulation	51.25	07.00	-	2075.0	0.0520			17.00	
In Zone:	Г	OU S center 4										
1		Raised floors	R-19 generic floor	31.25	64.00	1	2000.0	0.0526			19.00	
		between units	insulation									5-3
In Zone:	D	OU SW 1										
1		Slab floor	Soil, Concrete, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	D	OU SE 1										200
1		Bottom floor slab	Soil, Concrete, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:		OU NE 1								777404		_
1		Bottom floor slab	Soil, Concrete,	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
T 77		ATT NITE 4	carpet/pad									
In Zone:	L	OU NW 1										

1	Bottom floor slab	Soil, Concrete, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU N center 1	•									
1	Slab floor	Soil, Concrete, carpet/pad	31.25	67.00	1	2093.8	0.2725	29.33	110.00	3.67	
In Zone:	DU S center 1										100
1	Slab floor	Soil, Concrete, carpet/pad	31.25	64.00	1	2000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU N 2,3 center										200
1	raised floor between units	R-19 generic floor insulation	31.25	67.00	1	2093.8	0.0526			19.00	
In Zone:	DUS 2,3 center										
1	raised floor	R-19 generic floor insulation	31.25	64.00	1	2000.0	0.0526			19.00	
In Zone:	DU SW 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU SE 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU NW 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU NE 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	Cor 4										
1	Floor in corridor space of 4th floor	R-19 generic floor insulation	6.00	128.00	1	768.0	0.0526			19.00	
In Zone:	Cor 1										
1	slab in corridor space	Soil, Concrete, carpet/pad	6.00	128.00	1	768.0	0.2725	29.33	110.00	3.67	
In Zone:	Cor 2,3	2006 3 4 Table 3 2 (10 Table 20).									
1	Raised floor in corridor spaces	R-19 generic floor insulation	6.00	128.00	1	768.0	0.0526			19.00	

## Systems

HP SW 4	heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.90				
4	Air Distribution System						
HP SE 4	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NE 4	heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NW 4	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System					$\overline{}$	

HP NC 4	Heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SC 4	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00			$\neg \neg$	
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System		-34-00-00-00-00-00-00-00-00-00-00-00-00-00				
HP SW 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00			$\overline{}$	
2	Heating System	40000.00	80.00			$\exists$	
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SE 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System					$\exists$	

HP NE 1	Heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NW 1	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 1		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00			$\neg \neg$	
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP NC 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00			$\overline{}$	
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50			$\Box$	
-4	Air Distribution System						
HP SC 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System					$\equiv$	

HP N2,3 C	Heat pump		Constant Volume Air Cooled Split System < 65000 Btu/hr				
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP \$ 2,3 C	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 4		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SW 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System						
HP SE 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2		
Component	Category	Capacity	Efficiency	IPLV			
1	Cooling System	18000.00	12.00				
2	Heating System	40000.00	80.00				
3	Air Handling System -Supply	750.00	0.50				
4	Air Distribution System					$\overline{\Box}$	

HP NW 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	40000.00	80.00			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NE 2,3	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	40000.00	80.00			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System		***			
HP Corr 4	Heat pump thru wall	Through the Single Pac	he wall AirConditi kage	oner	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60			
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			
HP Coor 1	HP thru wall	Through the Single Pac	he wall AirConditi kage	oner	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60			
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			

HP Corr.2,3	HP thru wall	Through the Single Pac	No. Of Units 4			
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60			
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			

		Plant			
Equipment	Category	Size	Inst.No	Eff.	IPLV

Water Heaters								
W-Heater Description	CapacityCap.Unit	I/P Rt.	Efficiency	Loss				
1 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
2 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
3 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	[			
4 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	1			
5 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
6 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
7 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
8 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
9 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
10 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
11 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
12 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
13 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
14 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
15 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
16 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
17 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
18 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				
19 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]				

20 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
21 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
22 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
23 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
24 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
25 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
26 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
27 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
28 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
29 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
30 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
31 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]
32 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]

Description	Category	No. of Luminaires	Watts per Luminaire	Area/Len/No. of units [sf/ft/No]	Control Type	Wattage [W]	
		Piping	g				
No Type		Operating Temperature [F]	Insulation Conductivity Btu-in/h.sf.I		Insulation Thickness [in]	Is Runout?	

			Fenestra	ation Used		
Name	Glass Type	No. of Panes	Glass Conductance [Btu/h.sf.F]	SHGC	VLT	

Base N Chicago	User Defined	2	0.4800	0.4900	0.5200	
window Base other	User Defined	2	0.3400	0.3400	0.5600	
Chicago window	THE STATE OF THE S		Ski Cutrona	1223 H * H153	Country stage of	NO 32

Materials Used										
Mat No	Acronym	Description	Only R-Value Used	RValue [h.sf.F/Btu]	Thickness [ft]	Conductivity [Btu/h.ft.F]	Density [lb/cf]	SpecificHeat [Btu/lb.F]		
151	Matl151	CONC HW, DRD, 140LB, 4IN	No	0.4403	0.3333	0.7570	140.00	0.2000		
178 1015	Matl178 ApLbMatl015	CARPET W/RUBBER PAD Soil, 1 ft	Yes No	1.2300 2.0000	1.0000	0.5000	100.00	0.2000		

Constructs Used											
No	Name			Simple Construct	Massless Construct	Conductano [Btu/h.sf.F		Density [lb/cf]	RValue [h.sf.F/Btu]		
1062	R-13 wall 16 OC Ashrae App		No	Yes	0.09			11.2			
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor				
	1	1013	R-13 wall 16 OC A	ASHRAE App.			0.000				
No	Name			Simple Construct	Massless Construct	Conductano [Btu/h.sf.F		Density [lb/cf]	RValue [h.sf.F/Btu]		
1063	Steel exterior do	or ASHRAE	App	No	Yes	0.50			2.0		
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor				
	1	288	Steel exterior door	ASHRAE App	40		0.000				

No	Name			Simple Construct	Massless Construct	Conducta Btu/h.sf		Density [lb/cf]	RValue [h.sf.F/Btu]	
1064	Soil, Concrete,	carpet/pad		No	No	0.27	29.33	110.00	3.7	
	Layer	Material No.	Material			Thickness [ft]	Framing Factor			
	1	1015	Soil, 1 ft			1.0000	0.000			
	2	151	CONC HW, DRD,	140LB, 4IN		0.3333	0.000			
	3	178	CARPET W/RUBI	BER PAD			0.000			
No	Name			Simple Construct	Massless Construct	Conducta [Btu/h.sf		Density [lb/cf]	RValue [h.sf.F/Btu]	
1068	plywood roof 5	/8"		No	Yes	0.81			1.2	
	Layer	Material No.	Material			Thickness [ft]	Framing Factor			
	1	1010	PLYWOOD, 5/8IN	1		0.0521	0.000			
	2	1011	ASPHALT-SHING	LE AND SID	ING	0.0200	0.000			
No	Name			Simple Construct	Massless Construct	Conducta [Btu/h.sf		Density [lb/cf]	RValue [h.sf.F/Btu]	
1069	Attic gable end	wall		No	Yes	1.58			0.6	
	Layer	Material No.	Material			Thickness [ft]	Framing Factor			
	1	244	PLYWOOD, 1/2IN	1		0.0417	0.000			

## HOUSTON

No	Name			Simple Construct	Massless Construct	Conductano [Btu/h.sf.F		Density [lb/cf]	RValue [h.sf.F/Btu]	
1069	Attic gable end v	vall		No	Yes	1.58			0.6	
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor			
	1	244	PLYWOOD, 1/2I	N	(	0.0417	0.000			
No	Name			Simple Construct	Massless Construct	Conductano [Btu/h.sf.F		Density [lb/cf]	RValue [h.sf.F/Btu]	
1070	ASHRAE Appen	dix roof R-3	38	No	Yes	0.03			37.0	
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor			
	1	1012	R-38 roof truss A	SHRAE App.			0.000			
No	Name			Simple Construct	Massless Construct	Conductano [Btu/h.sf.F]		Density [lb/cf]	RValue [h.sf.F/Btu]	1
1071	R-19 generic floo	or insulation		No	Yes	0.05			19.0	
	Layer	Material No.	Material		Т	hickness [ft]	Framing Factor			
	1	1014	R-19 Generic Inst	ılation	(	0.4147	0.000			

# EnergyGauge Summit v3.11 INPUT DATA REPORT

## **Project Information**

Project Name: Baseline MF Houston Orientation: North

Project Title: Code minimum apartment in Houston Building Type: Multi-Family

Address: Enter Address here Building Classification: New Finished building

Enter Address here

State: Tx No.of Storeys: 4

Zip: 0 GrossArea: 44517 SF

Owner: NMHC

			Zones				
No	Acronym	Description	Туре	Area [sf]	Multiplier	Total Area [sf]	
1	Elevator zones	Elevator areas with mechanical space	UNCONDITIONED	96.0	1	96.0	
2	Attic	Attic	UNCONDITIONED	8973.5	1	8973.5	
3	DU SW 4	Dwelling unit SW corner on 4th story	CONDITIONED	1000.0	1	1000.0	
4	DU SE 4	Dwelling unit SE corner on 4th story	CONDITIONED	1000.0	1	1000.0	

5	DU NE 4	Dwelling unit on 4th floor at NE corner	CONDITIONED	1000.0	1	1000.0	
6	DU NW 4	Dwelling unit on 4th floor	CONDITIONED	1000.0	1	1000.0	
7	DUN center 4	at NW corner North DUs on 4th floor in	CONDITIONED	2093.8	1	2093.8	
		center					100-00
8	DU S center 4	South DUs on 4th floor in center	CONDITIONED	2000.0	1	2000.0	
9	DU SW 1	Dwelling unit SW corner on 1st story	CONDITIONED	1000.0	1	1000.0	
10	DU SE 1	Dwelling unit SE corner	CONDITIONED	1000.0	1	1000.0	
11	DU NE 1	on 1st story Dwelling unit on 1st floor at NE corner	CONDITIONED	1000.0	1	1000.0	
12	DU NW 1	Dwelling unit on 1st floor at NW corner	CONDITIONED	1000.0	1	1000.0	
13	DU N center 1	North DUs on 1st floor in center	CONDITIONED	2093.8	1	2093.8	
14	DU S center 1	South DUs on 1st floor in center	CONDITIONED	2000.0	1	2000.0	
15	DU N 2,3 center	Interior North DUs on 2nd and 3rd floors	CONDITIONED	4187.5	1	4187.5	
16	DU S 2,3 center	Interior south DUs on 2nd and 3rd floors	CONDITIONED	4000.0	1	4000.0	
17	DU SW 2,3	Dwelling unit SW corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
18	DU SE 2,3	Dwelling unit SE corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
19	DU NW 2,3	Dwelling unit NW corner on 2nd and 3rd story	CONDITIONED	2000.0	1	2000.0	
20	DU NE 2,3	Dwelling unit NE corner	CONDITIONED	2000.0	1	2000.0	
21	Cor 4	on 2nd and 3rd story 4th floor corridor	CONDITIONED	768.0	1	768.0	
22	Cor 1	1st floor corridor	CONDITIONED	768.0	1	768.0	
23	Cor 2,3	2nd, 3rd floor corridors	CONDITIONED	1536.0	1	1536.0	

	Spaces										
No	Acronym	Description	Туре	Depth [ft]	Width [ft]	Height [ft]	Multi plier	Total Area [sf]	Total Volume [cf]	-	
In Zone		combined elevator and	Electrical Mechanical Equipment Room - General	8.00	12.00	35.00	1	96.0	3360.0		
In Zone	: Attic attic space	attic space with average height assumed	Storage & Warehouse - Inactive Storage	68.50	131.00	8.50	1	8973.5	76274.8		
In Zone		individual dwelling unit	Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		
In Zone: DU SE 4  1 DU SE 4 DU 4th floor SE Private Living Space 31.25 32.00 8.00 1 1000.0 8000.0											
In Zone: DU NE 4  1 DU NE 4 DU on NE corner of Private Living Space 31.25 32.00 8.00 1 1000.0											
In Zone	DU NW 4		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008		
In Zone			Private Living Space	31.25	33.50	8.00	2	2093.8	16750.0		
In Zone			Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0		
In Zone	: DU SW I DU SE I		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008		
In Zone	: DU SE 1 DU SE 1		Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008		
In Zone	: DU NE 1 DU NE 1	DU on NE corner of 1st	Private Living Space	31.25	32.00	8.00	1	1000.0	0.0008		
In Zone	: DU NW DU NW 1	story  1  DU on NW corner of 1st story	Private Living Space	31.25	32.00	8.00	1	1000.0	8000.0		

In Zone			D	21.25	22.50	0.00		2002.0	16750.0	
1	DU N center	1 DU north in center of 1st story	Private Living Space	31.25	33.50	8.00	2	2093.8	16750.0	ш
In Zone	: DUS cer									
		oDU south in center of 1st story	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	: DU N 2,3									
1	DU interior N	loDUs in interior of 2nd and 3rd follrs	Private Living Space	31.25	33.50	8.00	4	4187.5	33500.0	
In Zone		utDUs center 2nd and	Private Living Space	31.25	32.00	8.00	4	4000.0	32000.0	
		3rd floors								
In Zone	DU SW 2,3	2,3 individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	DU SE 2.3	,3 individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	П
		•					1.75			
In Zone		2,3 individual dwelling unit	Private Living Space	31.25	32.00	8.00	2	2000.0	16000.0	
In Zone	DU NE 2,3	2,3 individual dwelling unit	Drivota Living Space	31.25	32.00	8.00	2	2000.0	16000.0	П
		maividuai awening unit	riivate Living Space	31.23	32.00	0.00	2	2000.0	10000.0	ш.
In Zone	Corridor 4	Corridor space on 4th floor	Corridor	128.00	6.00	8.00	1	768.0	6144.0	
In Zone	: Cor 1	11001								
Service and the service		eCorridor space	Corridor	128.00	6.00	8.00	1	768.0	6144.0	
In Zone	Corr 2,3	Corridor space 2,3 floors	Corridor	128.00	6.00	8.00	2	1536.0	12288.0	

Lighting										
No	Type	Category	No. of Luminaires	Watts per Luminaire	Power [W]	Control Type	No.of Ctrl pts			
	zones ator space Recessed Fluorescent - No vent	General Lighting	1	144	144	Manual On/Off	1			

In Zone: Atti	c								
In Space:	attic s	pace Incandescent	General Lighting	35	75	2625	Manual On/Off	4	
	SW 4								
In Space:	DU SI	E Roof Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:								1000	
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	NE 4								
In Space:	DU N	E 4 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NW 4 DU N								
2526	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	N cent								50-56
In Space:	DU N 1	center 4 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	S cent								
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	SW 1	3.1							
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	SE 1								<del>20-3</del> 3
In Space:	DU SI	E 1 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	

	72	537			120				
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	NE 1	oleven)							
In Space:	DU N	E 1 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	Principle of the Control of the Cont	6	7.5				
	-3.0		General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NW 1								
m space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N cen	ter 1							
In Space:		center 1 Compact Fluorescent	Consed Lighting	18	18	324	Manual On/Off		
	1		General Lighting					1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	S cent	ter 1 center bottom							
in space:	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	N 2,3	center							
In Space:	DU in	nterior North							
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
		center							
In Space:	DU co	enter south Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
	-77.0		General Lighting	0	00	300	Manual Off Off	1	
In Zone: DU In Space:	SW 2								
m space.	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU	SE 2,3	3							
In Space:	DU S	E 2,3		1947		1227	100 100 000		
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	

FOR STATE OF THE PARTY OF THE P	NW:								
In Space:	DU I	NW 2,3 Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: DU In Space:	NE 2								
	1	Compact Fluorescent	General Lighting	18	18	324	Manual On/Off	1	
	2	Incandescent	General Lighting	6	60	360	Manual On/Off	1	
In Zone: Co									
In Space:	Corr								
VIA.25	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	
In Zone: Co	r 1								
In Space:	Corr	ridor spaces							
•	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	
In Zone: Co	2,3								
In Space:	Corr	2,3							
•	1	Recessed Fluorescent - No vent	General Lighting	5	75	375	Manual On/Off	2	

					Walls	ý Ž					
No	Description	Туре	Width I [ft]	H (Effec) [ft]	Multi plier	Area [sf]	Direction	Conductance [Btu/hr. sf. F]	Heat Capacity [Btu/sf.F]	Dens. R-Value [lb/cf] [h.sf.F/Btu	]
In Z	Zone: Elevator zone	s									
1	East facing elevator wall 1st floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	East	0.0890		11.2	
2	East facing elevator wall 2.3 floor	R-13 wall 16 OC Ashrae App	12.00	8.00	2	96.0	East	0.0890		11.2	
3	East facing elevator wall 4th floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	East	0.0890		11.2	
4	West facing elevator wall 1st floor	R-13 wall 16 OC Ashrae App	12.00	8.00	1	96.0	West	0.0890		11.2	
5	West facing elevator wall 2,3 floor	R-13 wall 16 OC Ashrae App	12.00	8.00	2	96.0	West	0.0890		11.2	

	137 . C	R-13 wall 16 OC	10.00	8.00	-1	96.0	West	0.0890	11.0	П
6	West facing elevator wall		12.00	8.00	1	96.0	west	0.0890	11.2	ш
7	4th floor	Ashrae App	0.00	0.00	1	64.0	NT 41	0.0000	11.0	
7	North facing elevator	R-13 wall 16 OC	8.00	8.00	1	64.0	North	0.0890	11.2	ш
	wall 1st floor	Ashrae App		0.00						_
8	North facing elevator	R-13 wall 16 OC	8.00	8.00	2	64.0	North	0.0890	11.2	
	wall 2,3 floors	Ashrae App								_
9	North facing elevator	R-13 wall 16 OC	8.00	8.00	1	64.0	North	0.0890	11.2	
20172	wall 4th floor	Ashrae App								
In Z										_
1	Attic gable end wall	Attic gable end wall	68.50	8.56	1	586.4	East	1.5827	0.6	
8553	facing east									_
2	Attic gable end wall	Attic gable end wall	68.50	8.56	1	586.4	West	1.5827	0.6	
	facing west									
In Z										
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
		Ashrae App								×
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
l	corridor	Ashrae App								
In Z										
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
l	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
In Z										
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	walls	Ashrae App								
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
		Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
	corridor	Ashrae App								
In Z	one: DU NW 4	***								
1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
	walls	Ashrae App								
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
(300)	walls	Ashrae App								
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	South	0.0890	11.2	
(2)	corridor	Ashrae App			550	77877575			237773	_
	COTTACT	Torrac Typ								

In Z	Zone: DU N center 4									0-8
1	North facing exterior walls	R-13 wall 16 OC Ashrae App	33.50	8.00	2	268.0	North	0.0890	11.2	
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11.2	
2780	between units	Ashrae App								_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
1270	between units	Ashrae App								
4	Wall between unit and	R-13 wall 16 OC	33.50	8.00	2	268.0	South	0.0890	11.2	
l	corridor	Ashrae App								
In Z	Lone: DU S center 4									_
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11.2	
	walls	Ashrae App								_
2	West facing walls	R-13 wall 16 OC Ashrae App	31.25	8.00	1	250.0	West	0.0890	11.2	
3	East facing walls	R-13 wall 16 OC Ashrae App	31.25	8.00	1	250.0	East	0.0890	11.2	
4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11.2	
	corridor	Ashrae App								
In Z	Cone: DU SW 1		22.00	12122		22.120.121.121		20200	222.020	_
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	1	256.0	South	0.0890	11.2	
2	West facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	1	250.0	West	0.0890	11.2	
3	Wall between unit and	R-13 wall 16 OC	32.00	8.00	1	256.0	North	0.0890	11.2	
100.000	corridor	Ashrae App								
In Z	Zone: DU SE 1									_
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	1	256.0	South	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
3	Wall between unit and corridor	Ashrae App R-13 wall 16 OC Ashrae App	32.00	8.00	1	256.0	North	0.0890	11.2	
In Z	Zone: DU NE 1	A CONTRACTOR OF THE CONTRACTOR								
1	North facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	1	256.0	North	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11.2	
3	Wall between unit and corridor	Ashrae App R-13 wall 16 OC Ashrae App	32.00	8.00	1	256.0	South	0.0890	11.2	
In Z	Cone: DU NW 1	APP								

1	North facing exterior	R-13 wall 16 OC	32.00	8.00	1	256,0	North	0.0890	11	2	$\Box$
1	walls	Ashrae App	32.00	0.00	1	250.0	ivolui	0.0070	11	. 2	_
2	West facing exterior	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	2	
170	walls	Ashrae App									
3	Wall between unit and	R-13 wall 16 OC	8.00	32.00	1	256.0	South	0.0890	11	.2	
	corridor	Ashrae App									_
In 2	Zone: DU N center	1									
1	North facing exterior	R-13 wall 16 OC	33.50	8.00	2	268.0	North	0.0890	11	2	
	walls	Ashrae App									
2	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
	between units	Ashrae App									
3	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11	.2	
	between units	Ashrae App									
4	Wall between unit and	R-13 wall 16 OC	27.50	8.00	2	220.0	South	0.0890	11	.2	
	corridor	Ashrae App									1.32
In Z	Zone: DU S center 1										
1	South facing exterior	R-13 wall 16 OC	32.00	8.00	2	256.0	South	0.0890	11	.2	
	walls	Ashrae App									_
2	East facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	East	0.0890	11	.2	
- 82	between units	Ashrae App	0.000								_
3	West facing walls	R-13 wall 16 OC	31.25	8.00	1	250.0	West	0.0890	11	.2	
	between units	Ashrae App	230022	12022	1020	22200		1012200		020	_
4	Wall between unit and	R-13 wall 16 OC	32.00	8.00	2	256.0	North	0.0890	11	.2	
I	corridor	Ashrae App									
53	Cone: DU N 2,3 cen		22.50	0.00		250.0		0.0000			_
1	North walls on interior	R-13 wall 16 OC	33.50	8.00	4	268.0	North	0.0890	11	.2	
	DUs	Ashrae App	21.25	0.00	•	250.0		0.0000		•	-
2	East facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11	. 2	
,	between units	Ashrae App	21.05	8.00	2	250.0	West	0.0000	11	^	
3	West facing walls between units	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	west	0.0890	11	. 2	ᄓ
4	Wall between unit and	R-13 wall 16 OC	27.50	8.00	4	220.0	South	0.0890	11	2	
4	corridor	Ashrae App	27.50	8.00	4	220.0	South	0.0690	11	. 4	ᄓ
In 2	Cone: DU S 2,3 cent										
1	North walls on interior	R-13 wall 16 OC	33.50	8.00	4	268.0	South	0.0890	11	2	
	DUs	Ashrae App	33.50	0.00	7	200.0	Doddi	0.0070	11		_
2	West facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	West	0.0890	11	2	
	rrest facilig walls	Ashrae App	31.23	0.00	2	250.0	VYVSU	0.0070	11	-	_
3	East facing walls	R-13 wall 16 OC	31.25	8.00	2	250.0	East	0.0890	11	2	
	Trans taking wans	Ashrae App	01.20	0.00	2	250.0	1.74.50	0.0070	11	. 2	_
		. made rapp									

4	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	4	256.0	North	0.0890	11.2	
In Z	one: DU SW 2,3	Asiliac App								
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC	31.25	8.00	2	250.0	West	0.0890	11.2	
3	Wall between unit and corridor	Ashrae App R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
In Z	one: DU SE 2,3									
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	East	0.0890	11.2	
3	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
In Z	one: DU NW 2,3									
1	North facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	West	0.0890	11.2	
3	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
In Z	one: DU NE 2,3	100000000 000 000 <del>000</del> 0								
1	South facing exterior walls	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	North	0.0890	11.2	
2	East facing exterior walls	R-13 wall 16 OC Ashrae App	31.25	8.00	2	250.0	East	0.0890	11.2	
3	Wall between unit and corridor	R-13 wall 16 OC Ashrae App	32.00	8.00	2	256.0	South	0.0890	11.2	
In Z	one: Cor 4	romac ripp								
1	corridor end wall facing	R-13 wall 16 OC Ashrae App	6.00	8.00	1	48.0	East	0.0890	11.2	
2	Corridor wall facing west	R-13 wall 16 OC Ashrae App	6.00	8.00	1	48.0	West	0.0890	11.2	
In 7	one: Cor 1	Asinae App								
1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	1	48.0	East	0.0890	11.2	
2	east Corridor wall facing west	Ashrae App R-13 wall 16 OC	6.00	8.00	1	48.0	West	0.0890	11.2	
In Z	one: Cor 2,3	Ashrae App								

1	corridor end wall facing	R-13 wall 16 OC	6.00	8.00	2	48.0	East	0.0890	11.2	
2	east Corridor wall facing west	Ashrae App R-13 wall 16 OC Ashrae App	6.00	8.00	2	48.0	West	0.0890	11.2	

					Windo	ws						
	No	Description	Туре	Shaded	U [Btu/hr sf F]	SHGC	Vis.Tra	W [ft]	H (Effec) [ft]	Multi plier	Total Area [sf]	
In Zone: D In Wall:												
in wan:		North windows	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	Г
In Zone: D	U N ce	enter 1										_
In Wall:												_
	1	North windows	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	
In Zone: D												
In Wall:	N ext	Wall North windows	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	
In Zone: D			Oser Defined	110	0.4800	0.01	0.05	3.00	4.07	3	70.1	_
In Wall:		7										
	1	West windows,	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
		approx. 280 SF										•
In Wall:					0.4000	0.61		2.00		2	70.1	_
	1	North windows, approx. 70 SF	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	L
In Zone: D	HNE											
In Wall:												
	1	West windows,	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
		approx. 280 SF										
In Wall:		wall North windows	TT . D. C 1		0.4000	0.61	0.65	2.00	1.67	5	70.1	
	1		User Defined	No	0.4800	0.61	0.65	3.00	4.67	3	70.1	
In Zone: D In Wall:												
m wan.	1	West windows,	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	Г
		approx. 280 SF		2.0	011000	0.20	0.10	2.00				_
In Wall:	N ext											
	1	North windows,	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	
		approx. 70 SF										-

In Zone: DU NW 1										
In Wall: N ext wall				0.01		* * * *		19	=0.4	
<ol> <li>North windows, approx. 70 SF</li> </ol>	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	Ш
In Wall: W Ext walls										
<ol> <li>West windows, approx. 280 SF</li> </ol>	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
In Zone: DU NW 2,3										
In Wall: N ext wall										
<ol> <li>North facing windows</li> </ol>	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	
In Wall: W Ext walls										
<ol> <li>West windows, approx. 280 SF</li> </ol>	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
In Zone: DU NW 4										
In Wall: N ext wall										
<ol> <li>North windows, approx. 70 SF</li> </ol>	User Defined	No	0.4800	0.61	0.65	3.00	4.67	5	70.1	
In Wall: W Ext walls										_
1 West windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
In Zone: DU S 2,3 center										
In Wall: S Ext wall	100 10012 3	92223	8 1000	60000	5 22	12725	274227	100		_
<ol> <li>South windows</li> </ol>	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5	70.1	
In Zone: DU S center 1										
In Wall: S ext wall			0.4500	0.25	0.40	2.00	4.67	_	70.4	
1 South windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5	70.1	$\Box$
In Zone: DU S center 4										
In Wall: S ext wall  1 South windows	User Defined	NT-	0.4600	0.25	0.43	3.00	4.67	5	70.1	
	User Defined	No	0.4600	0.25	0.43	3.00	4.07	5	70.1	Ш
In Zone: DU SE 1 In Wall: E Ext walls										
1 West windows,	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
approx. 280 SF	Oser Defined	110	0.4000	0.23	0.43	5.00	4.07	3	42.0	ш
In Wall: S ext wall										
1 South windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5	70.1	
In Zone: DU SE 2,3										
In Wall: E Ext walls										
1 East windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	42.0	
In Wall: S ext wall										
1 South windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5	70.1	

In Zone: DU SE 4												
In Wall: E Ext	Walls East windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3		42.0	
In Wall: Sext v												ш
1	South windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5		70.1	
In Zone: DU SW 1												_
In Wall: Sext v	wall South windows	User Defined	Ma	0.4600	0.25	0.43	3.00	4.67	5		70.1	
In Wall: W Ext		Oser Defined	No	0.4000	0.25	0.43	3.00	4.07	3		70.1	ш
in wall: wext	West windows approx. 280 SF		No	0.4600	0.25	0.43	3.00	4.67	3	4	42.0	
In Zone: DU SW 2												
In Wall: S ext v												
1	South windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5		70.1	
In Wall: W ext			2002	12.71/2027	8202023	13. 425	12022	970227	- 23		102020	_
1	West windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	3	4	42.0	-
In Zone: DU SW 4 In Wall: S ext v	Contract to the contract to th											
1 wan. sext	South windows	User Defined	No	0.4600	0.25	0.43	3.00	4.67	5	- 1	70.1	
In Wall: W Ext			100000	100000000					1,75%			
1	West windows approx. 280 SF	<b>1</b> 000 - 1000 1000 1000 1000 1000 1000 10	No	0.4600	0.25	0.43	3.00	4.67	3	4	42.0	
				Doc	ors							
No Des	scription	Type	Shaded?		H (Effec)		Area	Cond.		Heat Cap.	R-Value	5
				[ft]	[ft]	plier	[sf] []	Btu/hr. sf. F]	[lb/cf]	[Btu/sf. F]	[h.sf.F/Btu	]
In Zone: DU SW 4												
In Wall: N		120 140		2.22		25	2111					-
1 en	try door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
		ASITICAE APP										
In Zone: DU SE 4		**										
In Zone: DU SE 4 In Wall: N	entry wall	••										
		Steel exterior door	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: N		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Wall: N	try door to unit		No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	

In Zone:	DU NW	7.4											
In	Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU N c	enter 4											
In	Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:													
In	Wall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU SW												
In	Wall:												
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU SE	1	D:0:										
In	Wall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU NE	1											
In	Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU NW	1											
In	Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU N c	enter 1											
In	Wall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DU S co	enter 1											
In	Wall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUN 2	,3 center	**										
		S entry wall											
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone:	DUS 2	3 center	7,000										
		N entry wall											

	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: D	USW	2.3	A SA										
	Vall:												
00.0296-1427	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: D	USE	2,3	6.6										
In W	Vall:	N entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: D	UNW	2,3											
In W	Vall:	S entry wall											
	1	entry door to unit	Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: D	U NE	2.3	Tr										
	Vall:	S entry wall											
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: C	or 4		потнаштър										
In W		E corr end											
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In W	Vall.	W corr end	. round as rep										
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: C	or 1		· · · · · · · · · · · · · · · · · · ·										
In W	Vall:	E corr end											
0.00	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In W	Vall:	W corr end	11										
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In Zone: C	or 2.3		11										
In W		E corr end											
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	
In W	Vall:	W corr end	TI										
	1		Steel exterior door ASHRAE App	No	3.00	6.67	1	20.0	0.5000	0.00	0.00	2.00	

					Roo	fs						
	No	Description	Туре	Width [ft]	H (Effec) [ft]	Multi plier	Area [sf]	Tilt [deg]	Cond. [Btu/hr. Sf. F]	Heat Cap I [Btu/sf. F] [	R-Value h.sf.F/Btu]	
In Zone:	1	Elevator zones roof over elevator	ASHRAE Appendix roof R-38	12.00	8.00	1	96.0	0.00	0.0270		37.0	
In Zone:	1	Attic South facing roof section	plywood roof 5/8"	34.25	128.00	1	4384.0	22.50	0.8137		1.2	
	2	North facing roof section	plywood roof 5/8"	34.25	131.00	1	4486.8	22.50	0.8137		1.2	
In Zone:	1	DU SW 4 roof-ceiling over SW corner DU	ASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	1	DU SE 4 roof-ceiling over corner SE DU	ASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	1	DU NE 4 roof-ceiling over NE DU	EASHRAE Appendix roof R-38	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	1	DU NW 4 roof-ceiling over NW corner DU	ASHRAE Appendix	32.00	31.25	1	1000.0	0.00	0.0270		37.0	
In Zone:	1	DU N center 4	ASHRAE Appendix roof R-38	31.25	67.00	1	2093.8	0.00	0.0270		37.0	
In Zone:	1	DU S center 4 roof-ceiling over corner DU	ASHRAE Appendix roof R-38	31.25	64.00	1	2000.0	0.00	0.0270		37.0	
In Zone:	1	Cor 4	ASHRAE Appendix roof R-38	6.00	128.00	1	768.0	0.00	0.0270		37.0	

				Skyl	ights								
	No Description Type U SHGC Vis.Trans W H (Effec) Multiplier Area Total Area [Btu/hr sf F] [ft] [ft] [Sf] [Sf]												
In Zone: In Roof:													

					Floors							
	No	Description	Туре	Width [ft]	H (Effec) [ft]	Multi plier		Cond. tu/hr. sf. F]	Heat Cap. [Btu/sf. F]		R-Value [h.sf.F/Btu]	
In Zone:	E	levator zones										
	1	Slab at bottom of elevator shaft	Soil, concrete, carpet/pad	8.00	12.00	1	96.0	0.2725	29.33	110.00	3.67	
In Zone:	A	ttic										
13	1	attic section overhanging smaller dwelling space	ASHRAE Appendix roof R-38	1.50	68.50	2	102.8	0.0270			37.04	
In Zone:	D	USW 4										
	1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U SE 4										
1	1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U NE 4										
1	1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U NW 4										_
	1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	D	U N center 4										
	1	Raised floors between units	R-19 generic floor insulation	31.25	67.00	1	2093.8	0.0526			19.00	
In Zone:	D	U S center 4										
	1	Raised floors between units	R-19 generic floor insulation	31.25	64.00	1	2000.0	0.0526			19.00	

In Zone:	DU SW 1 Slab floor	Soil, concrete,	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
		carpet/pad	52.00	31.23		1000.0	0.2723	27.55	110.00	5.07	
In Zone:	DU SE 1										100 000
1	Bottom floor slab	Soil, concrete, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU NE 1	A STATE OF THE STA									
1	Bottom floor slab	Soil, concrete, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU NW 1										
1	Bottom floor slab	Soil, concrete, carpet/pad	32.00	31.25	1	1000.0	0.2725	29.33	110.00	3.67	
In Zone:	DU N center 1	•									
1	Slab floor	Soil, concrete, carpet/pad	31.25	67.00	1	2093.8	0.2725	29.33	110.00	3.67	
In Zone:	DU S center 1										
1	Slab floor	Soil, concrete, carpet/pad	31.25	64.00	1	2000.0	0.2725	29.33	110.00	3.67	
In Zone	DU N 2,3 center	range reason									
1	raised floor between units	R-19 generic floor insulation	31.25	67.00	1	2093.8	0.0526			19.00	
In Zone:	DUS 2,3 center										
1	raised floor	R-19 generic floor insulation	31.25	64.00	1	2000.0	0.0526			19.00	
In Zone:	DU SW 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
T. 7		msulation									
1 Zone:	DU SE 2,3 Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	DU NW 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone	DU NE 2,3										
1	Raised floors between units	R-19 generic floor insulation	32.00	31.25	1	1000.0	0.0526			19.00	
In Zone:	Cor 4										
1	Floor in corridor	R-19 generic floor	6.00	128.00	1	768.0	0.0526			19.00	
	space of 4th floor	insulation	0.00	120.00	1	700.0	0.0520			19.00	
In Zone:		m 11			all a		0.0005	20.25			
1	slab in corridor space	Soil, concrete, carpet/pad	6.00	128.00	1	768.0	0.2725	29.33	110.00	3.67	Ц

In Zone:	Cor 2,3 Raised floor in	R-19 generic floor	6.00	128.00	1	768.0	0.0526	19.00	
	corridor spaces	insulation							

		Systems				
HP SW 4	heat pump	Constant System < 6	No. Of Units 1			
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP SE 4	Heat pump	Constant System < 6	No. Of Units 1			
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NE 4	heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					

HP NW 4	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NC 4	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP SC 4	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750,00	0.50			
4	Air Distribution System					
HP SW 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					$\overline{\Box}$

HP SE 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NE 1	Heat pump	Constant System < 6	No. Of Units 1			
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NW 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 1	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750,00	0.50			
4	Air Distribution System					
HP NC 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					$\overline{}$

HP SC 1	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP N2,3 C	Heat pump	Constant Volume Air Cooled Split System < 65000 Btu/hr			No. Of Units 4	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP S 2,3 C	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 4	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP SW 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					一

HP SE 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP NW 2,3	Heat pump	Constant System < 6	No. Of Units 2			
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			$\overline{\Box}$
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System		-3			
HP NE 2,3	Heat pump		Volume Air Cooled 55000 Btu/hr	Split	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	18000.00	12.00			
2	Heating System	18000.00	7.40			
3	Air Handling System -Supply	750.00	0.50			
4	Air Distribution System					
HP Corr 4	Heat pump thru wall	Through t Single Pac	he wall AirConditi kage	oner	No. Of Units 2	
Component	Category	Capacity	Efficiency	IPLV		
1	Cooling System	12000.00	10.60	_		
2	Heating System	12000.00	7.00			
3	Air Handling System -Supply	500.00	0.50			$\Box$

HP Coor 1	HP thru wall		Through the Single Packa	wall AirConditi age	oner	No. Of Units 2	
Component	Category		Capacity	Efficiency	IPLV		
1	Cooling System		12000.00	10.60			
2	Heating System		12000.00	7.00			
3	Air Handling System -Supply	M.	500.00	0.50			
HP Corr.2,3	HP thru wall		Through the Single Packa	wall AirConditi ge	ioner	No. Of Units 4	
Component	Category		Capacity	Efficiency	IPLV		
1	Cooling System		12000.00	10.60			
2	Heating System		12000.00	7.00			$\neg$
3	Air Handling System -Supply		500.00	0.50			
			Plant				
Equip	ment	Category	Size	Inst.No	Eff.	IPLV	
Equip	ment		S. Comm. (Communication of State Communication of State Communicatio	Inst.No	Eff.	IPLV	
	ment oter Description		Size	Inst.No	Eff.	IPLV Loss	
W-Hea		Wa	Size ter Heaters				
W-Hea  1 Gas Stora 2 Gas Stora	nter Description age water heater age water heater	CapacityCap.Unit  40 [Gal] 40 [Gal]	Size ter Heaters I/P Rt. 40000 [Btu/h] 40000 [Btu/h]	Efficiency 0.6200 0.6200	[Ef/Et]	Loss [Btu/h] [Btu/h]	
W-Hea  1 Gas Stora 2 Gas Stora 3 Gas Stora	ater Description age water heater age water heater age water heater	CapacityCap.Unit  40 [Gal] 40 [Gal] 40 [Gal]	Size  ter Heaters  I/P Rt.  40000 [Btu/h] 40000 [Btu/h] 40000 [Btu/h]	0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et]	Loss [Btu/h] [Btu/h] [Btu/h]	
W-Hea  1 Gas Stora 2 Gas Stora 3 Gas Stora 4 Gas Stora	age water heater age water heater age water heater age water heater age water heater	CapacityCap.Unit  40 [Gal] 40 [Gal] 40 [Gal] 40 [Gal] 40 [Gal]	Size  ter Heaters  I/P Rt.  40000 [Btu/h] 40000 [Btu/h] 40000 [Btu/h] 40000 [Btu/h]	0.6200 0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et]	Loss  [Btu/h] [Btu/h] [Btu/h] [Btu/h]	
W-Hea  1 Gas Stora 2 Gas Stora 3 Gas Stora 4 Gas Stora 5 Gas Stora	age water heater age water heater age water heater age water heater age water heater age water heater	CapacityCap.Unit  40 [Gal] 40 [Gal] 40 [Gal] 40 [Gal] 40 [Gal] 40 [Gal]	Size  ter Heaters  I/P Rt.  40000 [Btu/h] 40000 [Btu/h] 40000 [Btu/h] 40000 [Btu/h] 40000 [Btu/h]	0.6200 0.6200 0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et]	Loss  [Btu/h] [Btu/h] [Btu/h] [Btu/h] [Btu/h]	
W-Hea  1 Gas Stora 2 Gas Stora 3 Gas Stora 4 Gas Stora 5 Gas Stora 6 Gas Stora	age water heater age water heater	CapacityCap.Unit  40 [Gal]	Size  ter Heaters  I/P Rt.  40000 [Btu/h]	0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et]	Loss  [Btu/h] [Btu/h] [Btu/h] [Btu/h] [Btu/h]	
W-Hea  1 Gas Store 2 Gas Store 3 Gas Store 4 Gas Store 5 Gas Store 6 Gas Store 7 Gas Store	age water heater	CapacityCap.Unit  40 [Gal]	Size  L/P Rt.  40000 [Btu/h] 60000 [Btu/h]	0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et]	Loss  [Btu/h] [Btu/h] [Btu/h] [Btu/h] [Btu/h] [Btu/h]	
W-Hea  1 Gas Stora 2 Gas Stora 3 Gas Stora 4 Gas Stora 5 Gas Stora 6 Gas Stora 7 Gas Stora 8 Gas Stora	age water heater	CapacityCap.Unit  40 [Gal]	Size  L/P Rt.  40000 [Btu/h]	0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et]	Etw/h] [Btw/h] [Btw/h] [Btw/h] [Btw/h] [Btw/h] [Btw/h] [Btw/h]	
W-Hea  1 Gas Stora 2 Gas Stora 3 Gas Stora 4 Gas Stora 5 Gas Stora 6 Gas Stora 7 Gas Stora 8 Gas Stora 9 Gas Stora	age water heater	CapacityCap.Unit  40 [Gal]	Size  L/P Rt.  40000 [Btu/h] 60000 [Btu/h]	0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200 0.6200	[Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et] [Ef/Et]	Loss  [Btu/h] [Btu/h] [Btu/h] [Btu/h] [Btu/h] [Btu/h]	

12 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
13 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	┌
14 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
15 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
16 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
17 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
18 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
19 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
20 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
21 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
22 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
23 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
24 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
25 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
26 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
27 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
28 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
29 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
30 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
31 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	
32 Gas Storage water heater	40 [Gal]	40000 [Btu/h]	0.6200 [Ef/Et]	[Btu/h]	

Ext-Lighting										
Description	Category	No. of Luminaires	Watts per Luminaire	Area/Len/No. of units [sf/ft/No]	Control Type	Wattage [W]				
		Piping	g							
No Type		Operating Temperature [F]	Insulation Conductivity [ Btu-in/h.sf.]	y Diameter	Insulation Thickness [in]	Is Runout?				

Fenestration Used								
Name	Glass Type	No. of Panes	Glass Conductance [Btu/h.sf.F]	SHGC	VLT			
Base N Hou window	User Defined	2	0.4800	0.6100	0.6500			
Base other Hou window	User Defined	2	0.4600	0.2500	0.4300			

	Materials Used										
Mat No	Acronym	Description	Only R-Value Used	RValue [h.sf.F/Btu]	Thickness [ft]	Conductivity [Btu/h.ft.F]	Density [lb/cf]	SpecificHeat [Btu/lb.F]			
151	Matl151	CONC HW, DRD, 140LB, 4IN	No	0.4403	0.3333	0.7570	140.00	0.2000			
178 1015	Matl178 ApLbMat1015	CARPET W/RUBBER PAD Soil, 1 ft	Yes No	1.2300 2.0000	1.0000	0.5000	100.00	0.2000			

Constructs Used											
No	Name			Simple Construct	Massless Construct	Conductar [Btu/h.sf.]		Density [lb/cf]	RValue [h.sf.F/Btu]		
1062	R-13 wall 16 OC	R-13 wall 16 OC Ashrae App		No	Yes	0.09	120.10		11.2		
	Layer Material Material No.			Th	ickness [ft]	Framing Factor					
	1	1013	R-13 wall 16 OC	ASHRAE App.			0.000				

No	Name			Simple Construct	Massless Construct			eat Capacity [Btu/sf.F]	Density [lb/cf]	RValue [h.sf.F/Btu]	
1063	Steel exterior door ASHRAE App		No	Yes	0.50				2.0		
	Layer	Material No.	Material			Thickness [ft]	Framing Factor	<u>1</u>			
	1	288	Steel exterior door	ASHRAE App		107 1940	0.000				
No	Name			Simple Construct	Massless Construct			eat Capacity [Btu/sf.F]	Density [lb/cf]	RValue [h.sf.F/Btu]	
1064	Soil, concrete, car	rpet/pad		No	No	0.27		29.33	110.00	3.7	
-	Layer	Material No.	Material			Thickness [ft]	Framing Factor				
	1	151	CONC HW, DRD,	, 140LB, 4IN		0.3333	0.000				
	2	178	CARPET W/RUB	BER PAD			0.000				
	3	1015	Soil, 1 ft			1.0000	0.000				
No	Name			Simple Construct	Massless Construct		797G	eat Capacity [Btu/sf.F]	Density [lb/cf]	RValue [h.sf.F/Btu]	
1068	plywood roof 5/8	"		No	Yes	0.81			18-1	1.2	
	Layer	Material No.	Material			Thickness [ft]	Framing Factor	8			
	1	1010	PLYWOOD, 5/8IN	N		0.0521	0.000				
	2	1011	ASPHALT-SHING	GLE AND SIDI	NG	0.0200	0.000				

### APPENDIX C- REFERENCE VERSUS BASELINE BUILDING DISCUSSION

Although one might expect a building designed to the minimum prescriptive requirements in 90.1 to produce an energy cost budget similar to the reference building, this is not always the case. For example, the base building in Atlanta used 99.98% of the reference building energy cost budget. However, in Houston and Chicago, the base building was 93% to 94% of the reference design's energy cost budget.

Table 17 - Baseline versus reference energy cost budgets									
	Atla	anta	Chica	ago	Houston				
	Baseline	90.1	Baseline	90.1	Baseline	90.1			
	design	reference	design	reference	design	reference			
Total Cost									
Budget	\$32,942	\$32,946	\$52,691	\$56,951	\$60,742	\$64,960			
Electricity	\$32,942	\$32,946	\$22,949	\$25,323	\$60,742	\$64,960			
Area lights	\$6,299	\$6,895	\$6,535	\$6,746	\$12,746	\$13,175			
Misc. Equipment	\$4,733	\$4,733	\$4,636	\$4,630	\$9,044	\$9,044			
Pumps & Misc.	\$15	\$39	\$310	\$836	\$35	\$67			
Space cool	\$3,138	\$4,491	\$1,491	\$2,078	\$12,839	\$18,733			
Space heat	\$9,129	\$8,781	\$345	\$2,653	\$7,683	\$8,138			
Vent fans	\$9,627	\$8,007	\$9,632	\$8,380	\$18,396	\$15,804			
Natural gas			\$29,742	\$31,628					
Space heat			\$29,742	\$31,628					

Both the reference and baseline energy cost budgets are shown in Table 17. Normally, someone modeling a building to look at code compliance would only be concerned with being under the reference building energy cost budget. In our exercise, we had hoped that a building built to prescriptive minimums would yield something very close to the reference building, since one of our objectives was to then take that building and use it as a basis for later cost comparisons. This leaves open the argument that our costs to comply may be too high because theoretically we could have taken some of the insulation or other components out of our base building until it reached the same cost budget as the reference building.

However, the other side to this argument is that we would not be realistic if we based our costs on theoretical buildings, but should base them on current practice that meets today's code requirements. In fact, therein lies some of the explanation for how a prescriptive minimum building can score much lower than the reference building when using a performance approach. Taking windows as an example, there are no windows on the market that match up with both the U factor and SHGC specified in 90.1. In order to select a real window available within fairly conventional distribution channels, one usually ends up with a SHGC just under the 90.1 requirements but with a U factor much lower than required by the standard. This lowers the proposed design energy cost budget relative to the reference design.

Note that this outcome from simulations versus prescriptive requirements is not uncommon. Our experience with simulation tools on other buildings indicates that

running a simulation on a building that is slightly under the prescriptive minimums in a code can result in a passing score depending on the climate zone and building characteristics. Thus a design that is marginally deficient when looking at the prescriptive requirements can comply with a code simply by selecting another compliance path. Although we have not seen it, there may also be cases where a prescriptive compliant building fails a performance simulation check.

The end result of having a proposed base design coming in 5 or 6% under the reference building is that reaching a15%, 30% or 50% level of improvement is less of an uphill climb then it may first appear, although as shown in our simulation results it may still be difficult and costly to get there. As stated in the body of this report, this is partly due to a disconnect between minimum requirements in 90.1 and the characteristics of commercially available products. Today's standard practice already beats the code minimum in many cases.

### **APPENDIX D - DISCUSSION OF GSHP ESTIMATES**

Energy Gauge does not allow the user to model a GSHP. Thus, for the values in Tables 4, 5, and 6, we had to find an alternative approach for estimating the improvement in a building's performance due to a GSHP relative to the baseline building energy cost budget.

Unfortunately, there is no magic number or factor that one can use to represent the performance improvements of GSHP technology. Claims by industry groups and others have very broad ranges for the savings with this technology. Estimates on energy or cost savings range from 20% to higher than 50%. The technical literature also is lacking in this area.

There are at least two studies that provide detailed numbers on the expected improvement offered by GSHP technology. The first study was conducted in 1995 on 253 GSHPs (Lineau et. al., *Ground source heat pump case studies and utility programs*, Oregon Institute of Technology). In this study there was a fairly significant range of performance improvements identified with the systems, although the paper showed total heating and cooling costs were reduced with a GSHP an average of 31% compared to an air source heat pump and 18% compared to a gas furnace.

In the second project from the early 2000s, detailed monitoring of homes with GSHPs in the Cleveland area showed a 32% savings compared to a gas furnace and separate electric AC (NAHB Research Center, 2002, summarized at www.toolbase.org/Home-Building-Topics/Energy-Efficiency/Bob-Schmitt-Homes).

Even between these two very thorough studies, there is not much consistency, most likely because they involved different weather conditions and varying efficiency levels for both the GSHPs and the gas and electric systems they were using for comparison.

Because of the limitations with EG and the broad range of data in industry averages and the literature, we used a second simulation tool to estimate the impact of a GSHP. This allowed us to determine the percent improvement simulated in a given climate and apply these percentages to our baseline EG energy costs in that same climate. We subsequently applied the same process to a GSHP plus other changes to the building to see what the maximum improvement could be for the building.

The second simulation program - REM Design Version 12.42 from Architectural Energy Corporation – was selected for a number of reasons. REM Design was recently accredited by RESNET for use in assessing code compliance for the IECC. It is also the most widely used simulation tool by home energy raters.

REM Design is mostly used for single-family homes, but recent versions include the ability to model multi-family dwellings as either separate units in a building or as the entire building. Technically, it does not meet the 90.1 requirements for an acceptable simulation tool because it does not do hourly simulations. However, 90.1 does permit

use of other tools under special circumstances if approved by the local official. In this case, we believe it is reasonable to use REM Design to assess the potential of a GSHP.

#### **APPENDIX E - LIGHTING ISSUES**

Lighting can be a significant contributor to the overall energy use in a building. The way lighting electricity should be considered in a simulation is not completely clear in 90.1. Chapter 9 of the standard specifically exempts lighting within dwelling units from the requirements governing lighting. However, the requirements in Chapter 11 of 90.1 specify how lighting should be modeled in both the design and reference buildings, at least implying that it should be part of the energy cost budget method simulations. The developers of Energy Gauge included lighting in the simulations under the energy cost budget method.

We addressed lighting by assuming the Chapter 9 exemption for dwelling units in 90.1 does apply <u>and</u> that lighting should be included in the Energy Cost Budget simulation as implied in Chapter 11. To balance these two somewhat conflicting requirements, we set the lighting power in the design building as close as possible to the reference building. This allowed us to more accurately calculate heating and cooling loads, since they are influenced by lights, while at the same time the lighting loads balance each other out between the reference and design buildings.

The percent reduction due to a specific improvement in a building would change by a very slight amount if we had simply used zero lighting power inside the dwellings of both buildings, since the denominator used when calculating a percentage improvement would be smaller. However, the numerator would also decrease. This affect would occur with each simulation. Generally, each simulation result would vary by less than about 1%, although the relative difference would be even smaller between different simulations.

After weighing the pros and cons of the issue, we elected to keep the lighting in the energy cost budgets for both buildings. In our study, the potential variance in the % reduction for a specific improvement to the building is very small relative to the 50%, 30% or even 15% improvement we are trying to achieve. If our objectives were to explore small changes to the 90.1 requirements, we may have explored a different approach with lighting.